



**Stormwater Management Report
for
Touchstone Veterinary Center
382 Route 79**

Block 153, Lot 12

**Township of Marlboro
Monmouth County, New Jersey**

April 7, 2020

Prepared by:

A handwritten signature in black ink, appearing to read "M. Leber".

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Applicability of the Stormwater Management Rules (7:8-1.6)

The project will disturb in excess of one acre and proposes more than 1/4 of new impervious. Therefore, in accordance with N.J.A.C. 7:8-1.2 it is classified as a major development.

The purpose of this report is to demonstrate that the proposed development will comply with the peak rate of runoff, groundwater recharge, and water quality requirements of N.J.A.C. 7:8.

III. Hydrologic Methodology

In order to quantify the pre and post development peak rates of runoff, the Natural Resources Conservation Service (formerly SCS) TR-55 Method was used. The N.R.C.S. Method presents simplified procedures to calculate storm water runoff volume, peak rated of discharge, hydrographs, and storage volumes required for floodwater reservoirs. These procedures are applicable in small watersheds, especially urbanizing watersheds, in the United States.¹ The TR-55 model is generally used in analyzing watersheds under three (3) square miles (about 2,000 acres). The main parameters are described below:

CN = Curve Number. Based on soils, plant cover, amount of impervious areas, interception, and surface storage.

Tc = Time of Concentration. The time it takes from the most hydraulically distant point in a watershed to travel to a point of interest.

Lag Time = The distance from the center of mass of excess rainfall to the peak discharge. The lag equation is expressed as:

$$T_{lag} = \frac{L^{0.8} \times (S+1)^{0.7}}{1900 \times \sqrt{Y}}$$

L = length of the longest drainage path (feet)

S, the potential maximum retention of the soil in inches is expressed as:

$$S = (1000 / CN) - 10$$

Y = Average land slope (percent)

Empirically, the Lag Time has been expressed as 0.6Tc

A = Drainage Area (acres). The watershed area that contributes to the point of interest.

Rainfall = The 24-hour uniform rainfall amount imposed on the watershed. The rainfall amounts for Monmouth County, as revised in August 2012 are as follows:

<u>Storm Event</u>	<u>24-hour Rainfall (inches)</u>
1	2.79
2	3.38
5	4.38
10	5.23
25	6.53
100	8.94

¹ United States Department of Agriculture, Soil Conservation Service, Engineering Division, Technical Release 55

V. Post Development Drainage Conditions

This application results in an increase of impervious coverage. Therefore, a stormwater management system is proposed to attenuate the increase in peak rate of runoff leaving the site. The front developed portion of the site, the existing building, as well as the entire roof area of the proposed addition will drain into an above ground detention system. Part of the rear portion of the site (grass areas) will flow via overland flow into the basin, while the remaining areas will flow towards the brook.

In performing this analysis, East Point Engineering referred to the previously approved and constructed site plan for the adjacent northerly lot (386 Route 79). In order to ensure that no offsite runoff would be entering the new detention basin, the site plan for 386 Route 79 was overlayed onto the drainage area maps. The improvements installed at 386 Route 79 provided for a curb along 382 Route 79 as well as installation of an underground detention basin to serve their parking lot, driveway, and roof areas. A swale was proposed on the neighbors lot to convey offsite runoff in the wetlands thereby keeping offsite runoff from beyond 386 Route 79 out of their proposed underground detention system. Therefore, based on this analysis, there is no offsite runoff entering the proposed above ground detention basin at 382 Route 79.

Based on soils testing, the soils are classified as K3-K4 with an infiltration rate of 5.3 to 10.0 inches per hour. For the purposes of design, the assumed soil infiltration rate was 0.0 inches per hour.

The Post-Developed Drainage Area to the detention basin consists of the majority of the developed portion of the site, including roof and parking areas, which will be captured by a system of catch basins and inlets. The inflow hydrographs were separated out between pervious and impervious to better model the actual catchment area. Some overland areas will flow into the proposed detention basin. The hydrograph results are summarized below:

Proposed Condition – To Detention Basin 1 (Hydrograph 4)

Area = 0.53 acres
CN = 98 (impervious areas)
CN = 76 (pervious areas)
Tc = 10.0 minutes
2-yr. storm runoff = 1.28 cfs (5,404 C.F.)
10-yr. storm runoff = 2.08 cfs (8,888 C.F.)
100-yr. storm runoff = 3.72 cfs (16,057 C.F.)

Compliance with Runoff Quantity Requirements (7:8-5.4-3)

The N.J.D.E.P. regulates the runoff quantity requirements for Major Developments at N.J.A.C. 7:8-5.4(a)3. The rules permit an applicant to demonstrate compliance with the quantity requirements by selecting one (1) of the four (4) choices listed in subparts i. thru iv. These are provided below:

- i. Demonstrate through hydrologic and hydraulic analysis that for stormwater leaving the site, post-construction runoff hydrographs for the two, 10 and 100-year storm events do not exceed, at any point in time, the pre-construction runoff hydrographs for the same storm events;
- ii. Demonstrate through hydrologic and hydraulic analysis that there is no increase, as compared to the pre-construction condition, in the peak runoff rates of stormwater leaving the site for the two, 10 and 100-year storm events and that the increased volume or change in timing of stormwater runoff will not increase flood damage at or downstream of the site. This analysis shall include the analysis of impacts of existing land uses and projected land uses assuming full development under existing zoning and land use ordinances in the drainage area;
- iii. Design stormwater management measures so that the post-construction peak runoff rates for the two, 10 and 100-year storm events are 50, 75 and 80 percent, respectively, of the pre-construction peak runoff rates. The percentages apply only to the post-construction stormwater runoff that is attributable to the portion of the site on which the proposed development or project is to be constructed; or
- iv. In tidal flood hazard areas, stormwater runoff quantity analysis in accordance with (a)3i, ii and iii above shall only be applied if the increased volume of stormwater runoff could increase flood damages below the point of discharge.

Item i. above does not apply to the project. This choice is frequently selected when a site discharges to an isolated low area with no runoff leaving the site or when the net increase of impervious coverage is zero.

Item ii. above does not apply to the project since there will be a net increase of impervious surfaces.

Item iv. above does not apply to the project since the site is not located within a tidal flood hazard area.

Item iii. above is commonly known as the peak rate of runoff reductions or the "cutbacks". When a project proposes a net increase in impervious (pre vs post development) and a detention system is required, engineering designs demonstrate that this part of the rule is satisfied. **This is the portion of the regulations that is applicable to the project.**

Compliance with Water Quality Standards (7:8-5.5)

N.J.A.C. 7:8 states that water quality measures are applicable when greater than $\frac{1}{4}$ acre of new impervious surfaces are added. However, existing impervious areas are not subject to water quality requirements. Not all impervious surfaces are subject to water quality requirements. Roof runoff is considered clean, so is the runoff from patios and decks. For the subject site, water quality measures are applicable to the areas subject to new vehicular traffic only.

The project meets water quality as follows:

The portion of the site draining into the above ground detention basin has been routed with a minimal infiltration rate of 1.0 inch per hour and utilizing the water quality storm. In the analysis, there is no outflow from the basin and the depth of water in the basin is a maximum of 6-1/2 inches, which drains within 72 hours.

Appendix 1

Existing Runoff Calculations

Worksheet 3: Time of Concentration (T_c) or travel time (T_t)

Project 382 Route 79	By MSL	Date 7-Apr-20
Location Marlboro Township, Monmouth County	Checked BNP	Date 7-Apr-20
Check one: <input checked="" type="checkbox"/> Present <input type="checkbox"/> Developed		Existing D.A.
Check one: <input checked="" type="checkbox"/> T_c <input type="checkbox"/> T_t through subarea		
Notes: Space for as many as two segments per flow type can be used for each worksheet. Include a map, schematic or description of flow segments.		

Sheet Flow (Applicable to T_c only)

Segment ID	AB	GRASS	0.240	150	3.4	0.053	0.22	0.22
1. Surface description (table 3-1).....								
2. Manning's roughness coefficient, n (table 3-1).....								
3. Flow length, L (total L \leq 300 ft.).....	ft							
4. Two-year 24-hour rainfall, p_2	in							
5. Land slope, s	ft/ft							
6. $T_t = \frac{0.007(nL)^{0.8}}{P_2^{0.5} s^{0.4}}$ Compute T_t	hr	0.22	+			=	0.22	

Shallow Concentrated Flow

Segment ID	BC	UNPAVED	25	0.028	2.7	0.00	0.00	0.00
7. Surface description (paved or unpaved).....								
8. Flow Length, L.....	ft							
9. Watercourse slope, s.....	ft/ft							
10. Average velocity, V (figure 3-1).....	ft/s							
11. $T_t = \frac{L}{3600V}$ Compute T_t	hr	0.00	+			=	0.00	

Channel Flow

Segment ID								
12. Cross sectional flow area, a.....	ft ²							
13. Wetted perimeter, P_w	ft							
14. Hydraulic radius, $r=a/P_w$ Compute r.....	ft							
15. Channel slope, s.....	ft/ft							
16. Manning's roughness coefficient, n.....								
17. $V = \frac{1.49r^{2/3}\sqrt{s}}{n}$ Compute V.....	ft/s							
18. Flow length, L.....	ft							
19. $T_t = \frac{L}{3600V}$ Compute T_t	hr		+			=	0.00	
20. Watershed or subarea T_c or T_t (add T_t in steps 6, 11, and 19).....	hr							
	min							
							13.1	

Hydrograph Return Period Recap

Hydraflow Hydrographs by InteliSolve v9.23

Hyd. No.	Hydrograph type (origin)	Inflow Hyd(s)	Peak Outflow (cfs)								Hydrograph description
			1-Yr	2-Yr	3-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr	
1	SCS Runoff	-----	-----	1.593	-----	-----	3.061	-----	-----	6.070	Existing D.A.

Hydrograph Report

Hydraflow Hydrographs by Intelisolve v9.23

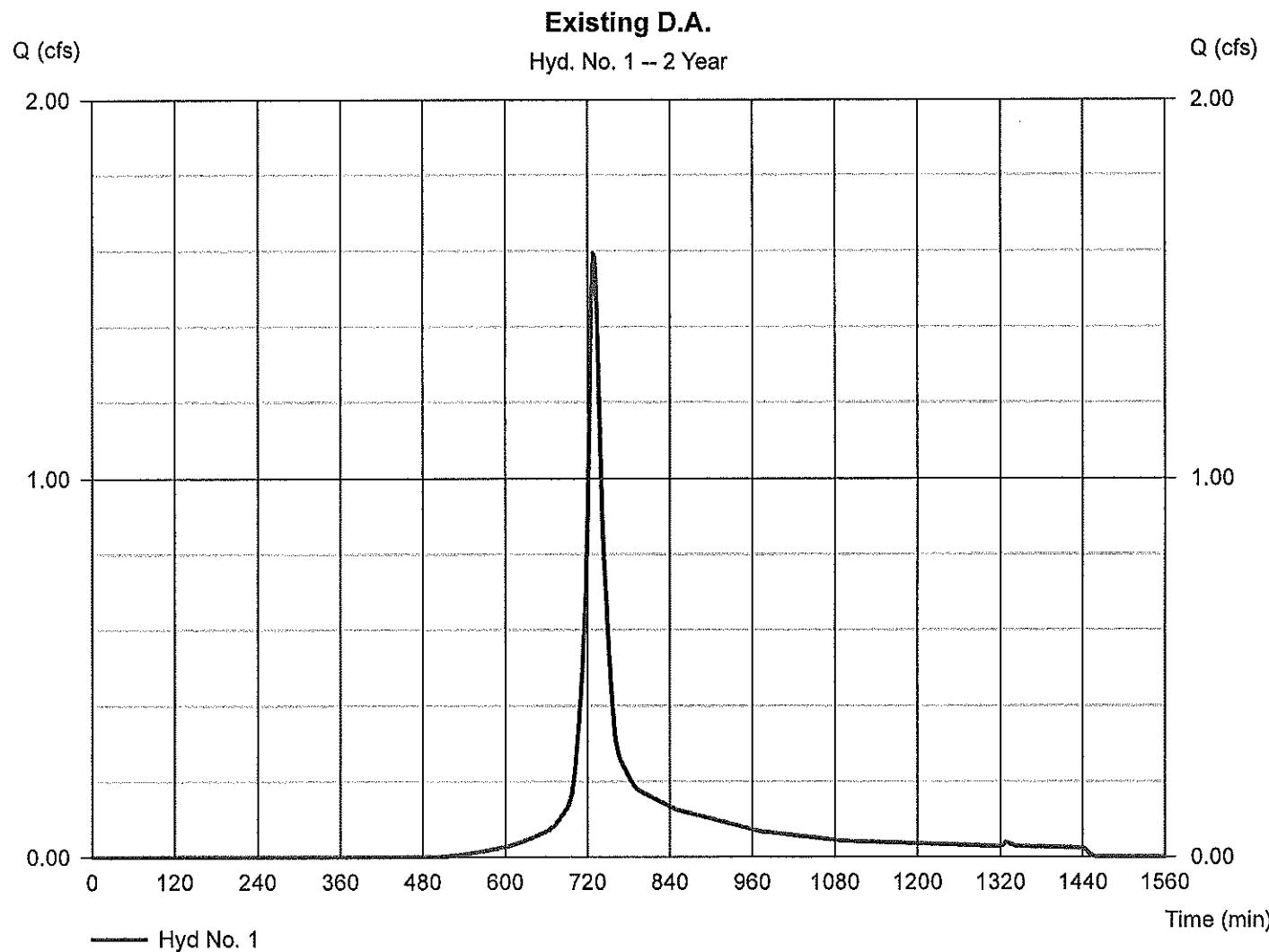
Thursday, May 14, 2020

Hyd. No. 1

Existing D.A.

Hydrograph type = SCS Runoff
 Storm frequency = 2 yrs
 Time interval = 2 min
 Drainage area = 0.930 ac
 Basin Slope = 0.0 %
 Tc method = USER
 Total precip. = 3.38 in
 Storm duration = 24 hrs

Peak discharge = 1.593 cfs
 Time to peak = 728 min
 Hyd. volume = 6,121 cuft
 Curve number = 83
 Hydraulic length = 0 ft
 Time of conc. (Tc) = 13.10 min
 Distribution = Type III
 Shape factor = 484



Hydrograph Report

Hydraflow Hydrographs by Intelsolve v9.23

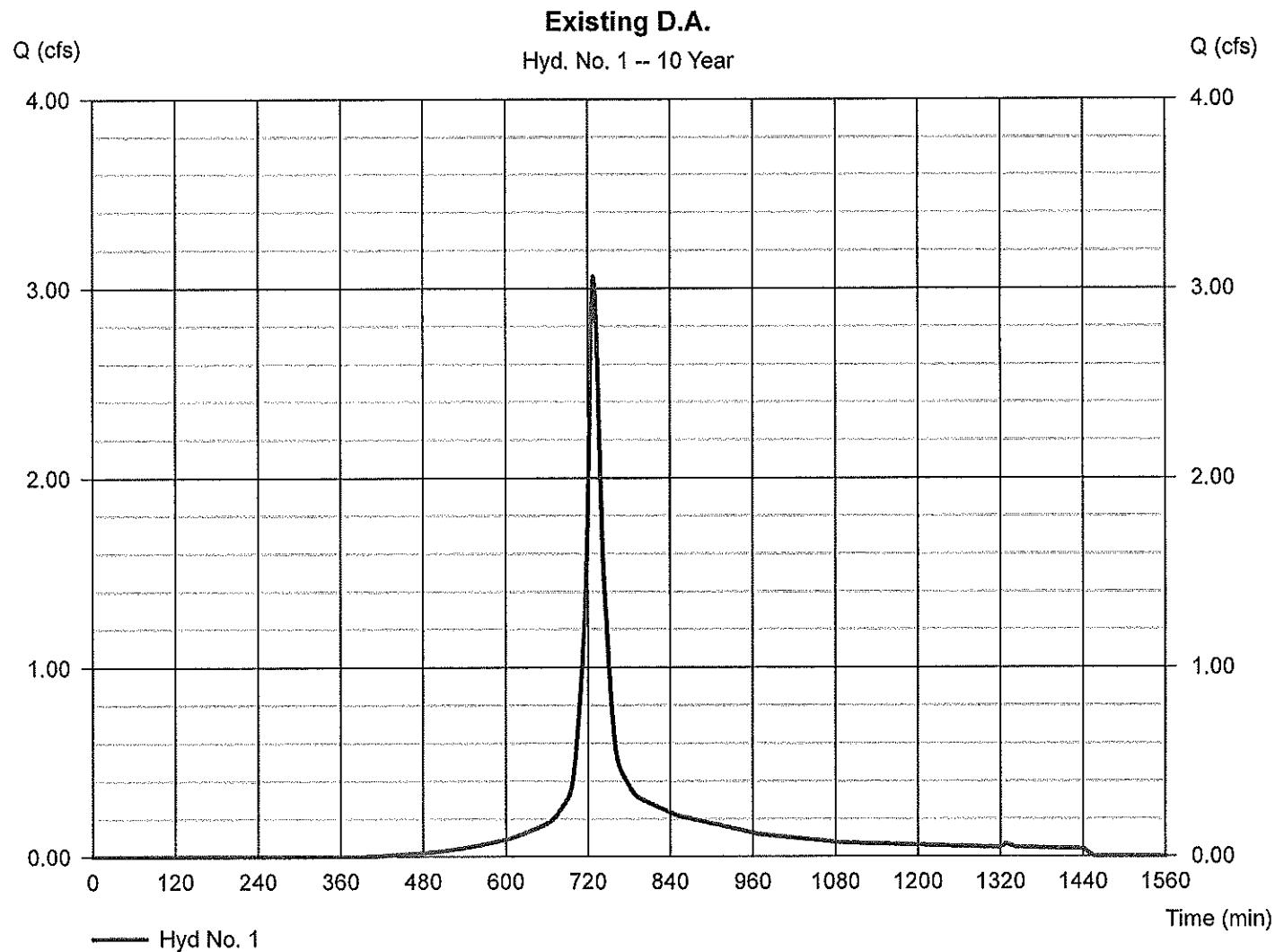
Thursday, May 14, 2020

Hyd. No. 1

Existing D.A.

Hydrograph type = SCS Runoff
 Storm frequency = 10 yrs
 Time interval = 2 min
 Drainage area = 0.930 ac
 Basin Slope = 0.0 %
 Tc method = USER
 Total precip. = 5.23 in
 Storm duration = 24 hrs

Peak discharge = 3.061 cfs
 Time to peak = 728 min
 Hyd. volume = 11,777 cuft
 Curve number = 83
 Hydraulic length = 0 ft
 Time of conc. (Tc) = 13.10 min
 Distribution = Type III
 Shape factor = 484



Hydrograph Report

Hydraflow Hydrographs by Intelsolve v9.23

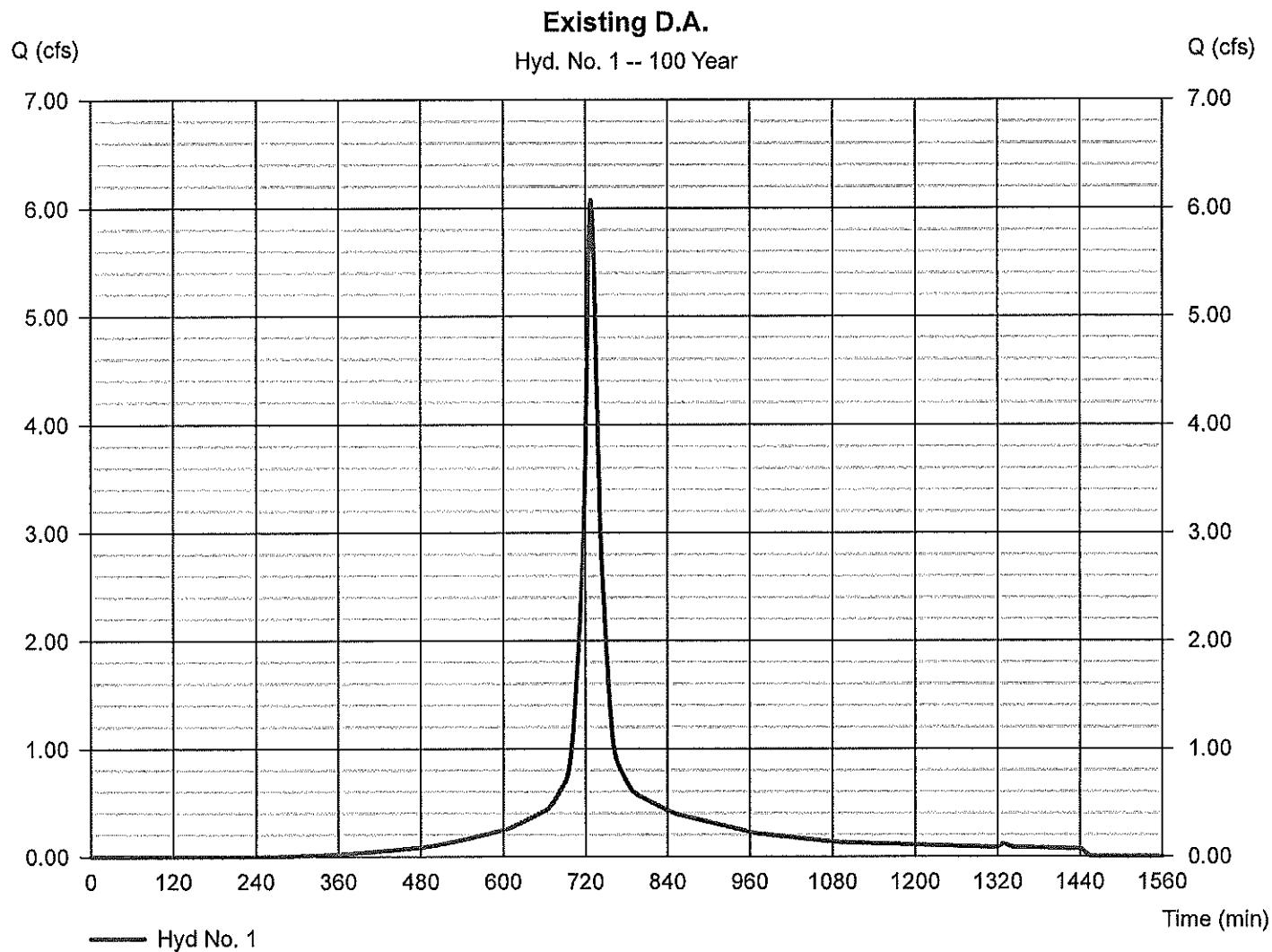
Thursday, May 14, 2020

Hyd. No. 1

Existing D.A.

Hydrograph type = SCS Runoff
 Storm frequency = 100 yrs
 Time interval = 2 min
 Drainage area = 0.930 ac
 Basin Slope = 0.0 %
 Tc method = USER
 Total precip. = 8.94 in
 Storm duration = 24 hrs

Peak discharge = 6.070 cfs
 Time to peak = 728 min
 Hyd. volume = 23,948 cuft
 Curve number = 83
 Hydraulic length = 0 ft
 Time of conc. (Tc) = 13.10 min
 Distribution = Type III
 Shape factor = 484



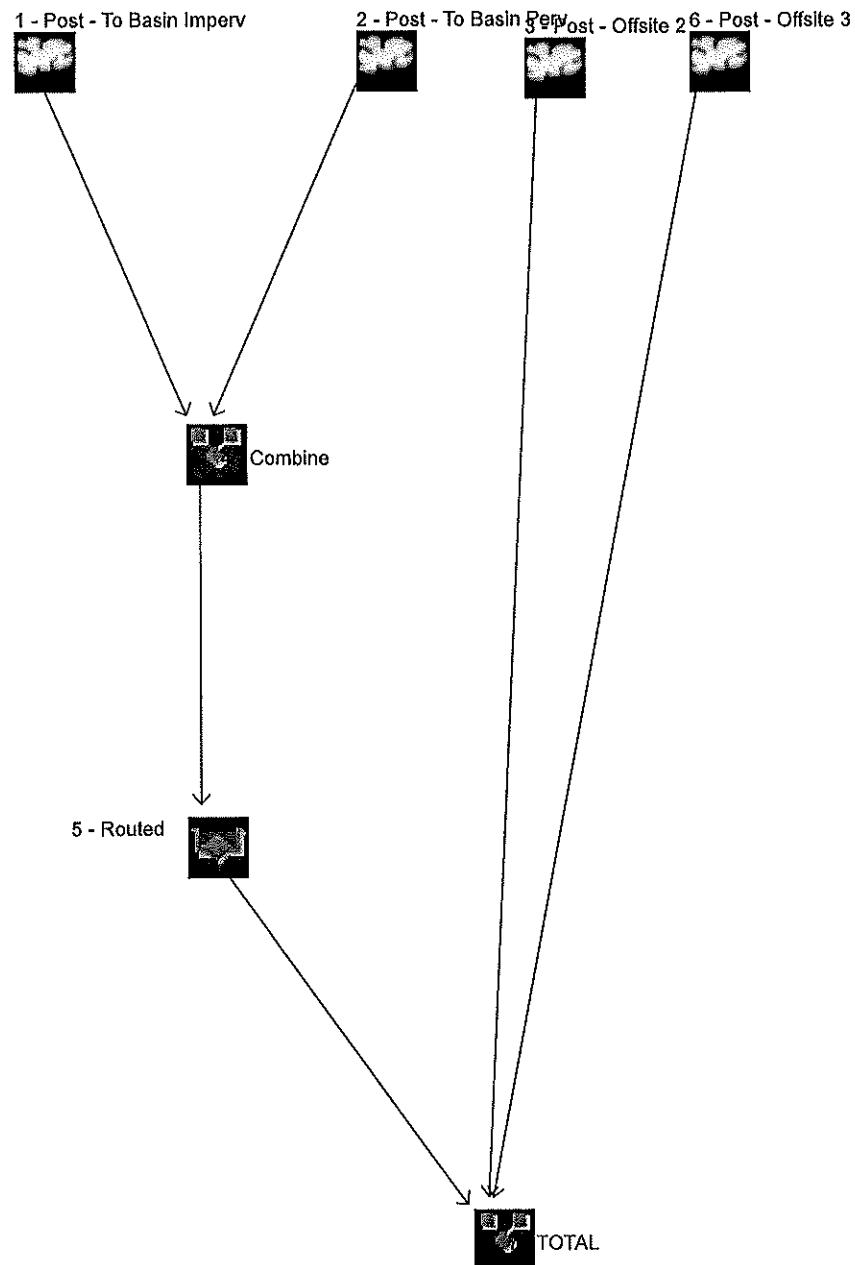
Worksheet 2: Runoff curve number and runoff

Project 382 Route 79		By MSL		Date 7-Apr-20						
Location Marlboro Township, Monmouth County		Checked BNP		Date 7-Apr-20						
Check one: <input type="checkbox"/> Present <input checked="" type="checkbox"/> Developed		Post-Developed D.A. 1 (To Basin, Imp)								
1. Runoff curve number										
Soil name and hydrologic group (appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	CN ¹		Area <table border="1"><tr><td>x</td><td>acres</td></tr><tr><td></td><td>m²</td></tr><tr><td></td><td>%</td></tr></table> Product of CN x Area	x	acres		m ²		%
		x	acres							
	m ²									
	%									
Table 2-2	Figure 2-3	Figure 2-4								
D	Roof Areas & Walkways	98		0.18 17.64						
D	Asphalt	98		0.21 20.58						
D	Grass / Open	80		0.00 0.00						
C	Impervious	98		0.02 1.96						
C	Grass / Open	74		0.00 0.00						
1. Use only one CN source per line		Totals →		0.41 40.18						
$\text{CN} \text{ (weighted)} = \frac{\text{tot.prod.}}{\text{tot. area}} = \frac{40.18}{0.410} = 98.0$; Use CN →		98						
2. Runoff										
	Storm #1	Storm #2	Storm #3							
	Frequency..... yr	2	10	100						
	Rainfall, P (24-hour).... in									
Runoff, Q..... in										
Use P and CN with table 2-1, figure										

Worksheet 2: Runoff curve number and runoff

Watershed Model Schematic

Hydraflow Hydrographs by InteliSolve v9.23



Legend

<u>Hyd. Origin</u>	<u>Description</u>
1 SCS Runoff	Post - To Basin Imperv
2 SCS Runoff	Post - To Basin Perv
3 SCS Runoff	Post - Offsite 2
4 Combine	Combine
5 Reservoir	Routed
6 SCS Runoff	Post - Offsite 3
7 Combine	TOTAL

Hydrograph Summary Report

Hydraflow Hydrographs by InteliSolve v9.23

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	1.131	2	728	4,830	---	---	---	Post - To Basin Imperv
2	SCS Runoff	0.145	2	730	575	---	---	---	Post - To Basln Perv
3	SCS Runoff	0.444	2	728	1,727	---	---	---	Post - Offsite 2
4	Combine	1.275	2	728	5,404	1, 2,	---	---	Combine
5	Reservoir	0.302	2	756	3,171	4	123.12	3,157	Routed
6	SCS Runoff	0.255	2	730	1,005	---	---	---	Post - Offsite 3
7	Combine	0.738	2	732	5,903	3, 5, 6	---	---	TOTAL
proposed 04-07-20.gpw				Return Period: 2 Year			Thursday, May 14, 2020		

Hydrograph Report

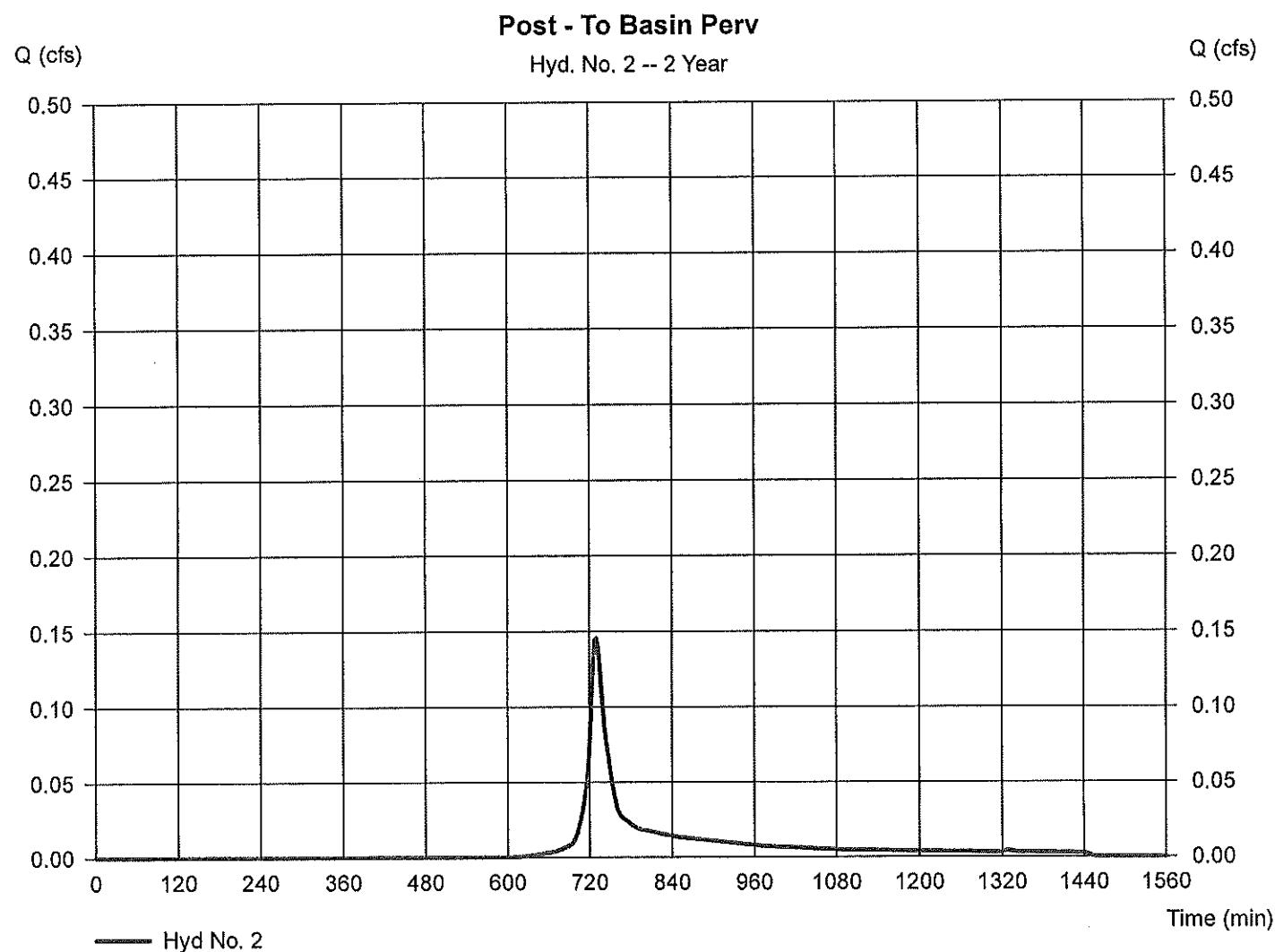
Hydraflow Hydrographs by intellisolve v9.23

Thursday, May 14, 2020

Hyd. No. 2

Post - To Basin Perv

Hydrograph type	= SCS Runoff	Peak discharge	= 0.145 cfs
Storm frequency	= 2 yrs	Time to peak	= 730 min
Time interval	= 2 min	Hyd. volume	= 575 cuft
Drainage area	= 0.120 ac	Curve number	= 76
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= USER	Time of conc. (Tc)	= 10.00 min
Total precip.	= 3.38 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydrograph Report

Hydraflow Hydrographs by Intellsolve v9.23

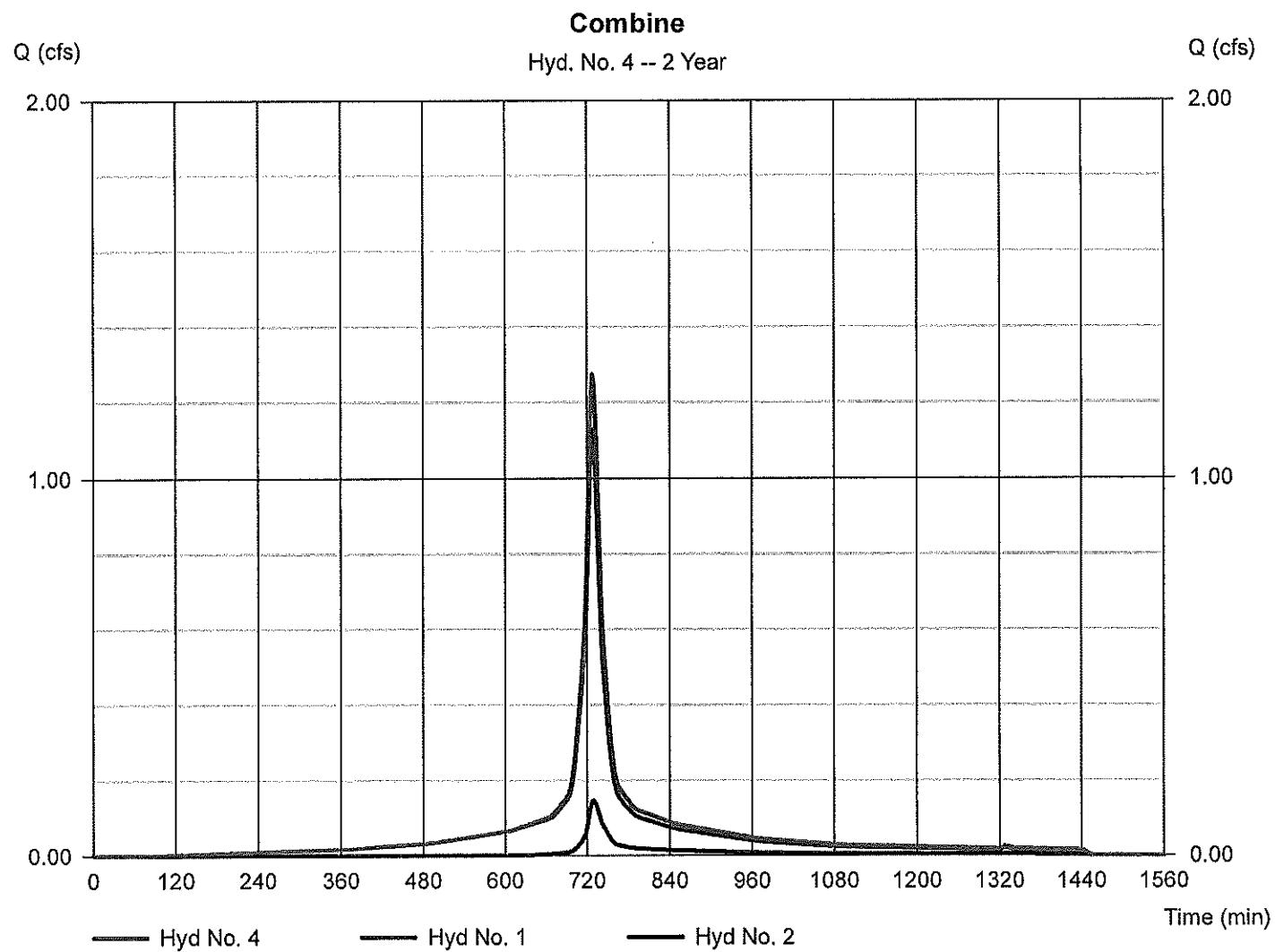
Thursday, May 14, 2020

Hyd. No. 4

Combine

Hydrograph type = Combine
 Storm frequency = 2 yrs
 Time interval = 2 min
 Inflow hyds. = 1, 2

Peak discharge = 1.275 cfs
 Time to peak = 728 min
 Hyd. volume = 5,404 cuft
 Contrib. drain. area = 0.530 ac



Pond Report

Hydraflow Hydrographs by Intellisolve v9.23

Thursday, May 14, 2020

Pond No. 1 - Basin

Pond Data

Contours - User-defined contour areas. Conic method used for volume calculation. Beginning Elevation = 121.95 ft

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	121.95	00	0	0
0.05	122.00	2,477	41	41
1.05	123.00	3,000	2,734	2,775
2.05	124.00	3,385	3,190	5,966

Culvert / Orifice Structures

Weir Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 0.00	0.00	0.00	0.00	Crest Len (ft)	= 0.50	10.00	0.00	0.00
Span (in)	= 0.00	0.00	0.00	0.00	Crest El. (ft)	= 122.80	123.90	0.00	0.00
No. Barrels	= 1	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 0.00	0.00	0.00	0.00	Weir Type	= Rect	Rect	---	---
Length (ft)	= 0.00	0.00	0.00	0.00	Multi-Stage	= No	No	No	No
Slope (%)	= 0.00	0.00	0.00	n/a	Exfil.(in/hr)	= 0.000 (by Wet area)			
N-Value	= .013	.013	.013	n/a	TW Elev. (ft)	= 0.00			
Orifice Coeff.	= 0.60	0.60	0.60	0.60					
Multi-Stage	= n/a	No	No	No					

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	121.95	--	--	--	--	0.00	0.00	--	--	--	--	0.000
0.01	4	121.96	--	--	--	--	0.00	0.00	--	--	--	--	0.000
0.01	8	121.96	--	--	--	--	0.00	0.00	--	--	--	--	0.000
0.02	12	121.97	--	--	--	--	0.00	0.00	--	--	--	--	0.000
0.02	17	121.97	--	--	--	--	0.00	0.00	--	--	--	--	0.000
0.03	21	121.98	--	--	--	--	0.00	0.00	--	--	--	--	0.000
0.03	25	121.98	--	--	--	--	0.00	0.00	--	--	--	--	0.000
0.04	29	121.99	--	--	--	--	0.00	0.00	--	--	--	--	0.000
0.04	33	121.99	--	--	--	--	0.00	0.00	--	--	--	--	0.000
0.04	37	122.00	--	--	--	--	0.00	0.00	--	--	--	--	0.000
0.05	41	122.00	--	--	--	--	0.00	0.00	--	--	--	--	0.000
0.15	315	122.10	--	--	--	--	0.00	0.00	--	--	--	--	0.000
0.25	588	122.20	--	--	--	--	0.00	0.00	--	--	--	--	0.000
0.35	861	122.30	--	--	--	--	0.00	0.00	--	--	--	--	0.000
0.45	1,135	122.40	--	--	--	--	0.00	0.00	--	--	--	--	0.000
0.55	1,408	122.50	--	--	--	--	0.00	0.00	--	--	--	--	0.000
0.65	1,682	122.60	--	--	--	--	0.00	0.00	--	--	--	--	0.000
0.75	1,955	122.70	--	--	--	--	0.00	0.00	--	--	--	--	0.000
0.85	2,229	122.80	--	--	--	--	0.00	0.00	--	--	--	--	0.000
0.95	2,502	122.90	--	--	--	--	0.05	0.00	--	--	--	--	0.053
1.05	2,775	123.00	--	--	--	--	0.15	0.00	--	--	--	--	0.149
1.15	3,044	123.10	--	--	--	--	0.27	0.00	--	--	--	--	0.274
1.25	3,413	123.20	--	--	--	--	0.42	0.00	--	--	--	--	0.421
1.35	3,732	123.30	--	--	--	--	0.59	0.00	--	--	--	--	0.589
1.45	4,051	123.40	--	--	--	--	0.77	0.00	--	--	--	--	0.774
1.55	4,370	123.50	--	--	--	--	0.98	0.00	--	--	--	--	0.975
1.65	4,689	123.60	--	--	--	--	1.19	0.00	--	--	--	--	1.191
1.75	5,009	123.70	--	--	--	--	1.42	0.00	--	--	--	--	1.422
1.85	5,328	123.80	--	--	--	--	1.66	0.00	--	--	--	--	1.665
1.95	5,647	123.90	--	--	--	--	1.92	0.00	--	--	--	--	1.921
2.05	5,966	124.00	--	--	--	--	2.19	1.05	--	--	--	--	3.242

Hydrograph Report

Hydraflow Hydrographs by InteliSolve v9.23

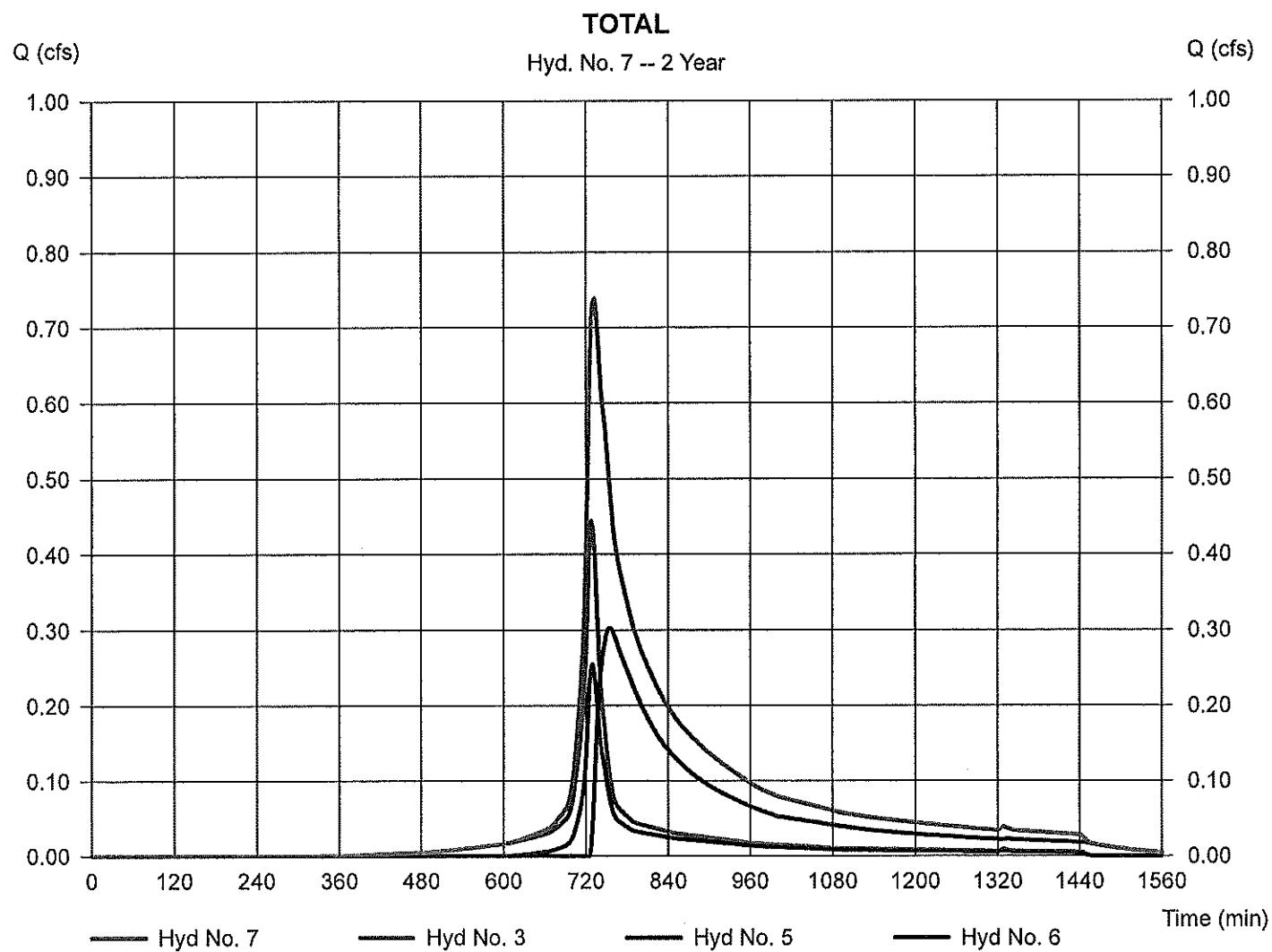
Thursday, May 14, 2020

Hyd. No. 7

TOTAL

Hydrograph type = Combine
Storm frequency = 2 yrs
Time interval = 2 min
Inflow hyds. = 3, 5, 6

Peak discharge = 0.738 cfs
Time to peak = 732 min
Hyd. volume = 5,903 cuft
Contrib. drain. area = 0.400 ac



Hydrograph Report

Hydraflow Hydrographs by Intellisolve v9.23

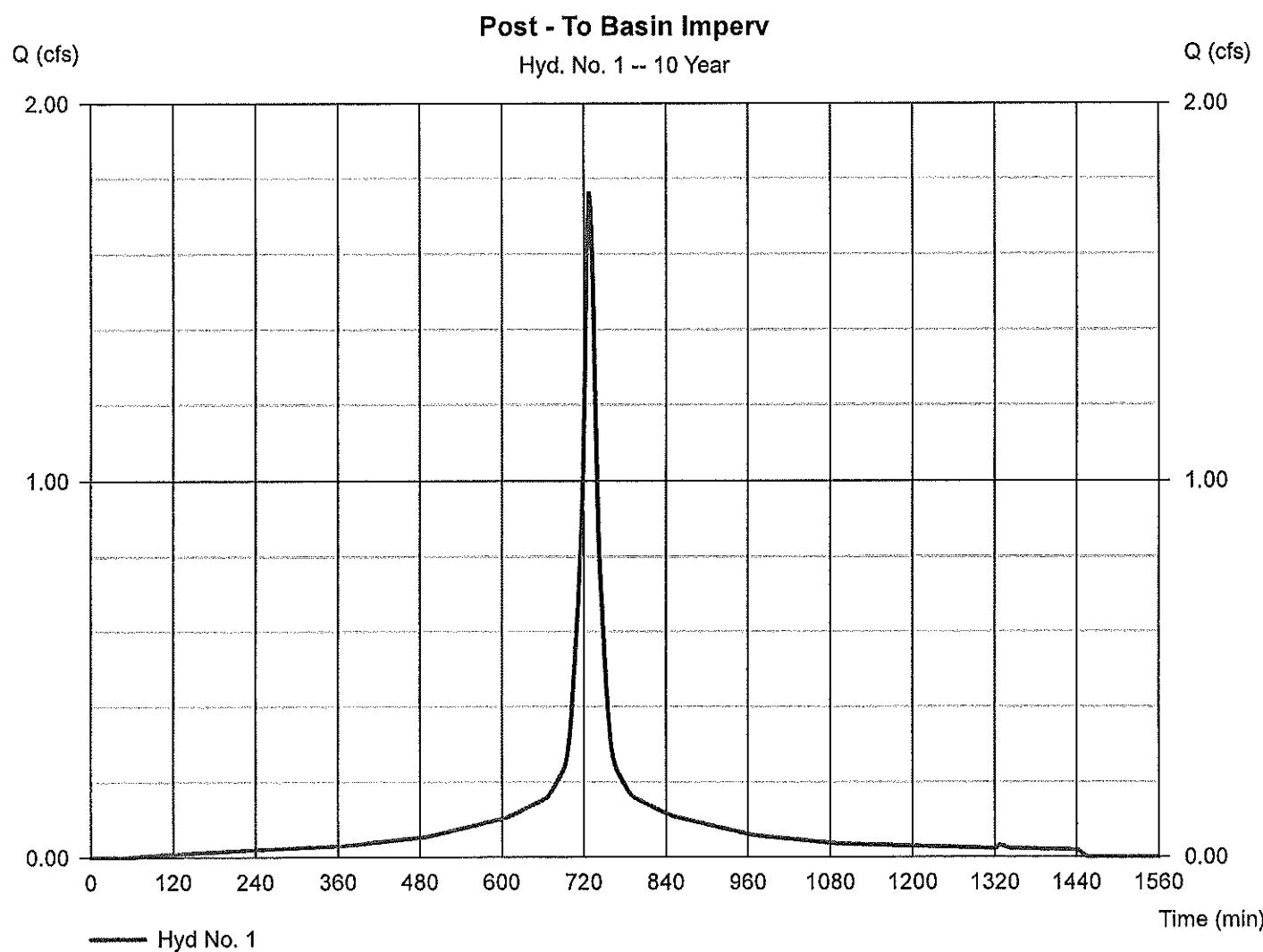
Thursday, May 14, 2020

Hyd. No. 1

Post - To Basin Imperv

Hydrograph type = SCS Runoff
 Storm frequency = 10 yrs
 Time interval = 2 min
 Drainage area = 0.410 ac
 Basin Slope = 0.0 %
 Tc method = USER
 Total precip. = 5.23 in
 Storm duration = 24 hrs

Peak discharge = 1.762 cfs
 Time to peak = 728 min
 Hyd. volume = 7,663 cuft
 Curve number = 98
 Hydraulic length = 0 ft
 Time of conc. (Tc) = 10.00 min
 Distribution = Type III
 Shape factor = 484



Hydrograph Report

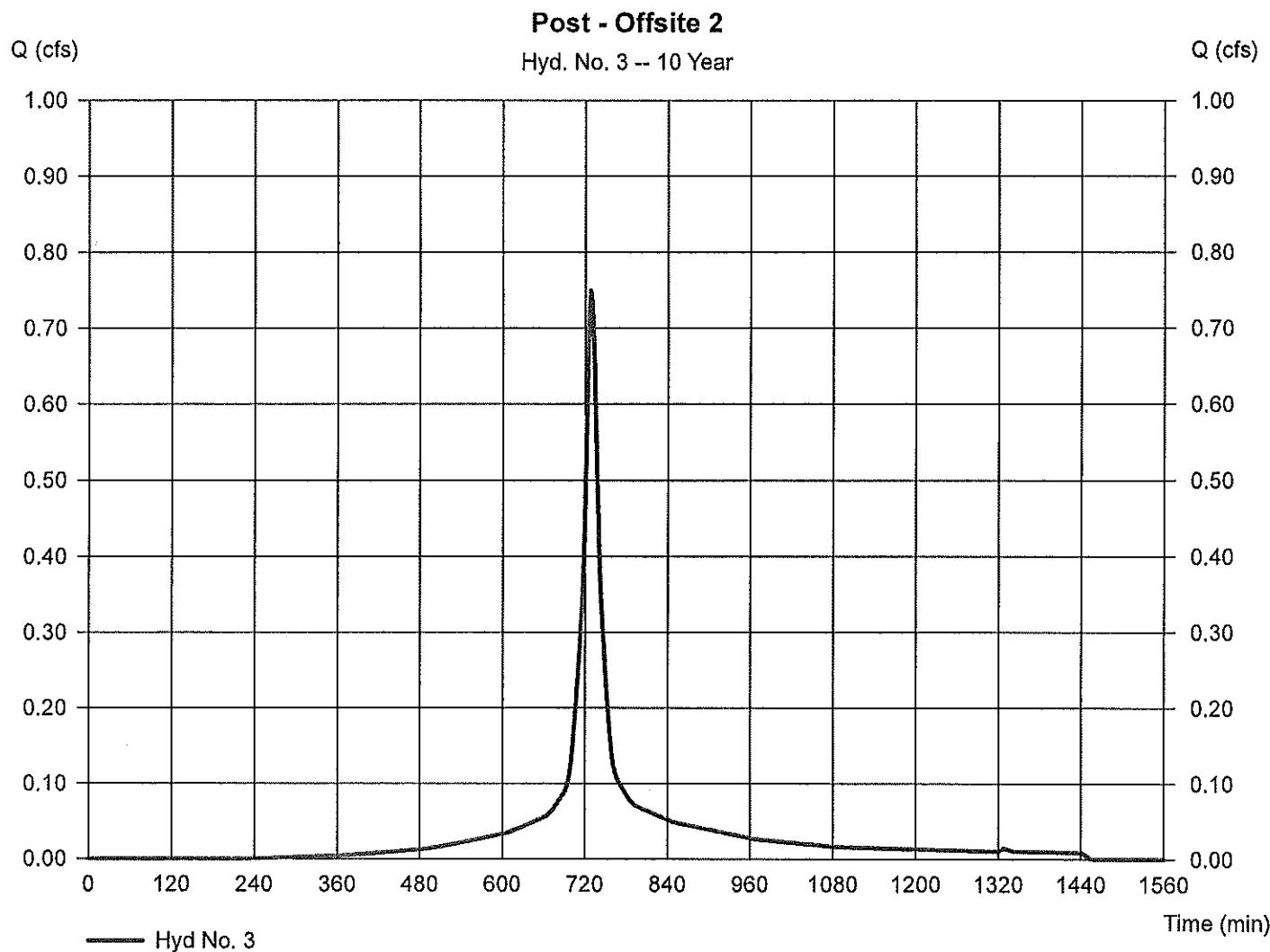
Hydraflow Hydrographs by InteliSolve v9.23

Thursday, May 14, 2020

Hyd. No. 3

Post - Offsite 2

Hydrograph type	= SCS Runoff	Peak discharge	= 0.749 cfs
Storm frequency	= 10 yrs	Time to peak	= 728 min
Time interval	= 2 min	Hyd. volume	= 2,991 cuft
Drainage area	= 0.190 ac	Curve number	= 91
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= USER	Time of conc. (Tc)	= 10.00 min
Total precip.	= 5.23 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydrograph Report

Hydraflow Hydrographs by InteliSolve v9.23

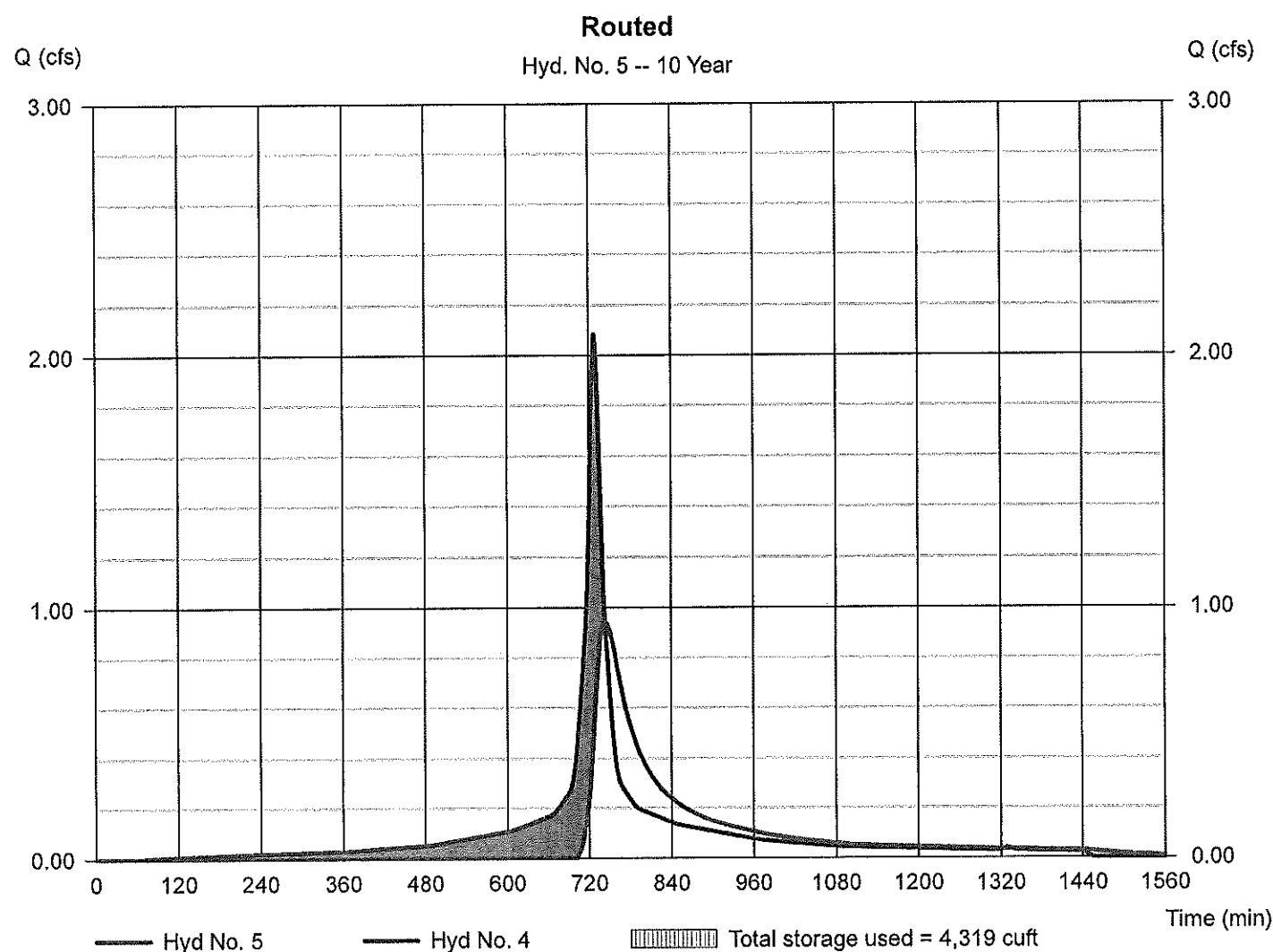
Thursday, May 14, 2020

Hyd. No. 5

Routed

Hydrograph type	= Reservoir	Peak discharge	= 0.943 cfs
Storm frequency	= 10 yrs	Time to peak	= 744 min
Time interval	= 2 min	Hyd. volume	= 6,654 cuft
Inflow hyd. No.	= 4 - Combine	Max. Elevation	= 123.48 ft
Reservoir name	= Basin	Max. Storage	= 4,319 cuft

Storage Indication method used.



Hydrograph Report

Hydraflow Hydrographs by Intellsolve v9.23

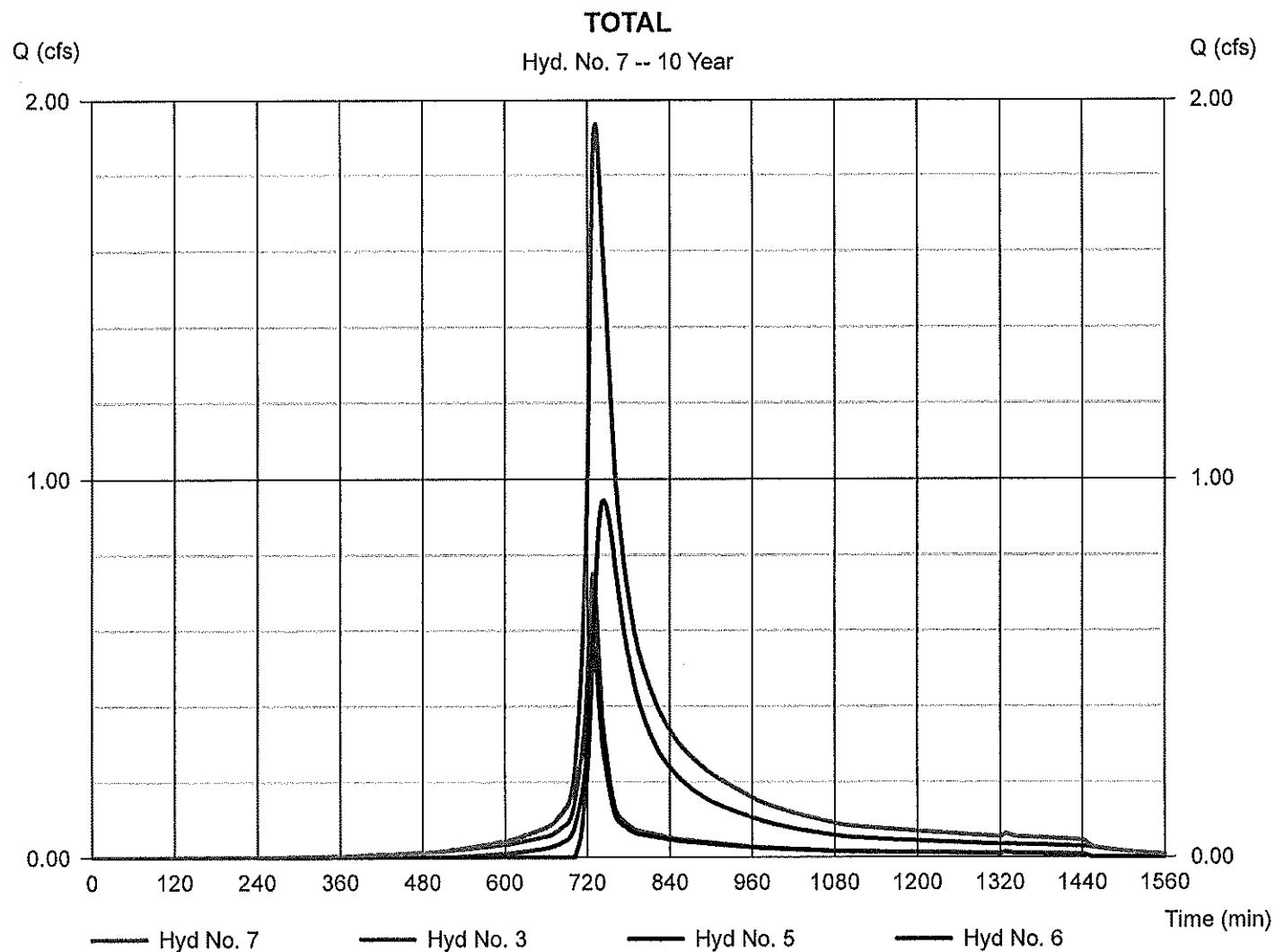
Thursday, May 14, 2020

Hyd. No. 7

TOTAL

Hydrograph type = Combine
 Storm frequency = 10 yrs
 Time interval = 2 min
 Inflow hyds. = 3, 5, 6

Peak discharge = 1.936 cfs
 Time to peak = 732 min
 Hyd. volume = 11,788 cuft
 Contrib. drain. area = 0.400 ac



Hydrograph Report

Hydraflow Hydrographs by Intellisolve v9.23

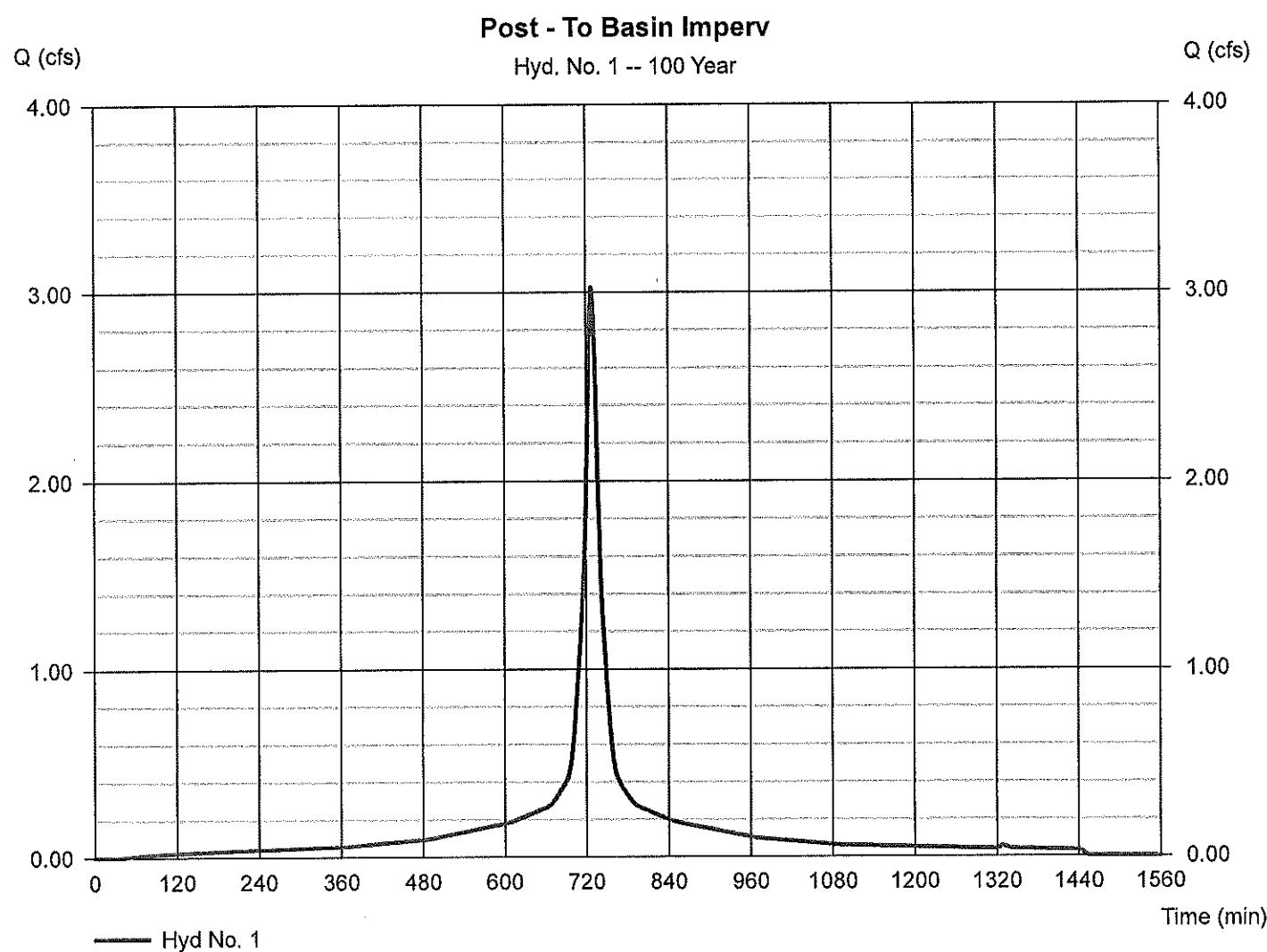
Thursday, May 14, 2020

Hyd. No. 1

Post - To Basin Imperv

Hydrograph type = SCS Runoff
 Storm frequency = 100 yrs
 Time interval = 2 min
 Drainage area = 0.410 ac
 Basin Slope = 0.0 %
 Tc method = USER
 Total precip. = 8.94 in
 Storm duration = 24 hrs

Peak discharge = 3.023 cfs
 Time to peak = 728 min
 Hyd. volume = 13,352 cuft
 Curve number = 98
 Hydraulic length = 0 ft
 Time of conc. (Tc) = 10.00 min
 Distribution = Type III
 Shape factor = 484



Hydrograph Report

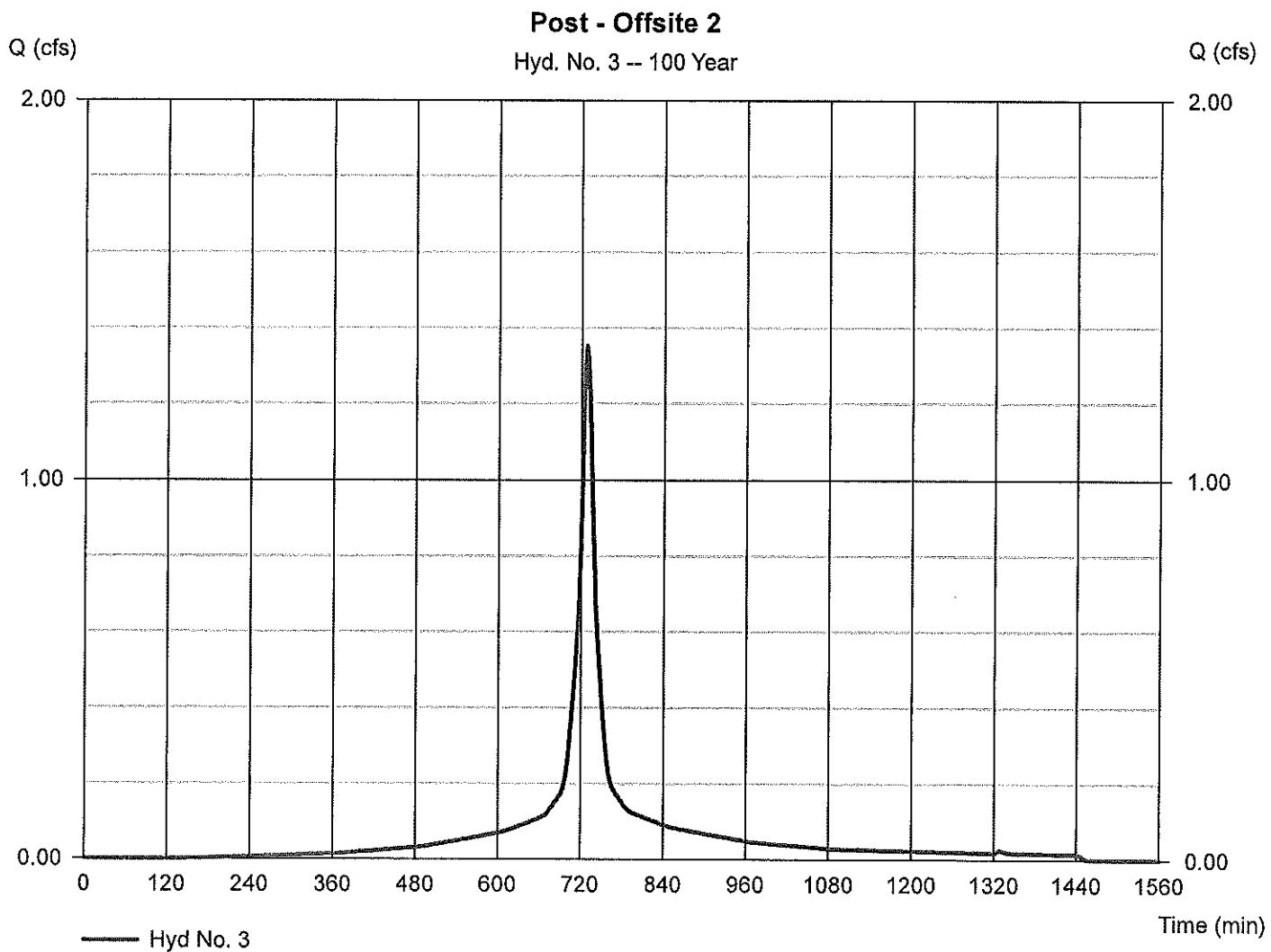
Hydraflow Hydrographs by InteliSolve v9.23

Thursday, May 14, 2020

Hyd. No. 3

Post - Offsite 2

Hydrograph type	= SCS Runoff	Peak discharge	= 1.352 cfs
Storm frequency	= 100 yrs	Time to peak	= 728 min
Time interval	= 2 min	Hyd. volume	= 5,586 cuft
Drainage area	= 0.190 ac	Curve number	= 91
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= USER	Time of conc. (Tc)	= 10.00 min
Total precip.	= 8.94 in	Distribution	= Type III
Storm duration	= 24 hrs	Shape factor	= 484



Hydrograph Report

Hydraflow Hydrographs by Intellsolve v9.23

Thursday, May 14, 2020

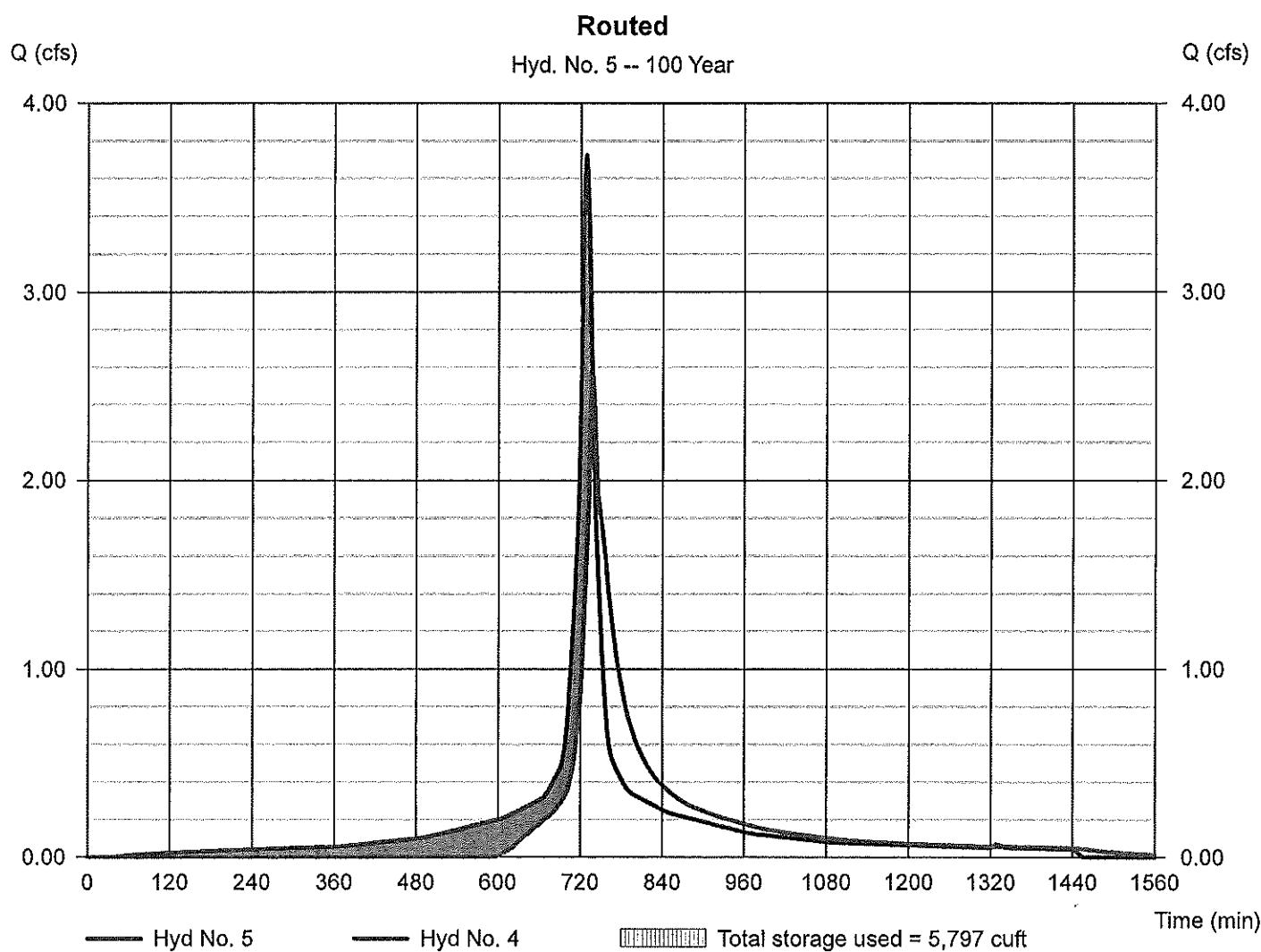
Hyd. No. 5

Routed

Hydrograph type = Reservoir
 Storm frequency = 100 yrs
 Time interval = 2 min
 Inflow hyd. No. = 4 - Combine
 Reservoir name = Basin

Peak discharge = 2.545 cfs
 Time to peak = 738 min
 Hyd. volume = 13,823 cuft
 Max. Elevation = 123.95 ft
 Max. Storage = 5,797 cuft

Storage Indication method used,



Hydrograph Report

Hydraflow Hydrographs by Intellisolve v9.23

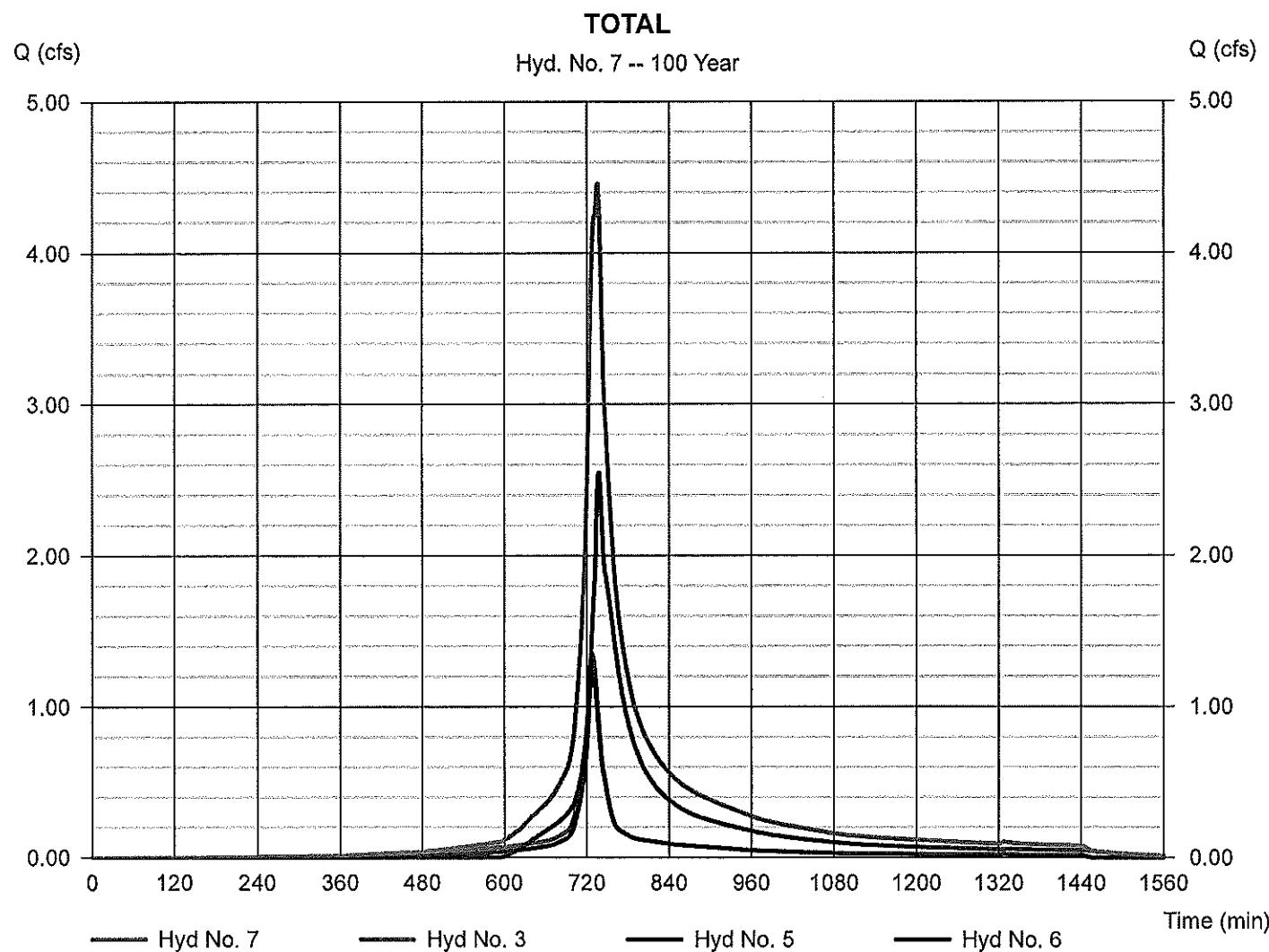
Thursday, May 14, 2020

Hyd. No. 7

TOTAL

Hydrograph type = Combine
 Storm frequency = 100 yrs
 Time interval = 2 min
 Inflow hyds. = 3, 5, 6

Peak discharge = 4.457 cfs
 Time to peak = 736 min
 Hyd. volume = 24,142 cuft
 Contrib. drain. area = 0.400 ac



Soil Map—Monmouth County, New Jersey
(NRCS Soil Survey - 382 Route 79)



Map Scale: 1:840 if printed on A landscape (11" x 8.5") sheet.
0 10 20 30 40 50 60 Meters
0 40 80 120 160 200 Feet

Map projection: Web Mercator Corner coordinates: WGS84 Edge ticks: UTM Zone 18N WGS84

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
KemB	Keyport sandy loam, 2 to 5 percent slopes	0.9	46.9%
KkgkB	Klej loamy sand, clayey substratum, 0 to 5 percent slopes	0.1	4.6%
ShrA	Shrewsbury sandy loam, 0 to 2 percent slopes	0.9	48.5%
Totals for Area of Interest		1.9	100.0%



Hydrologic Soil Group—Monmouth County, New Jersey
(NRCS Soil Survey - 382 Route 79)

MAP LEGEND

Area of Interest (AO)	Area of interest (AO)	C	C/D
Soils		D	
			Not rated or not available
Soil Rating Polygons	A		
	A/D		
	B		
	B/D		
	C		
	C/D		
	D		
	Not rated or not available		
Water Features			
Streams and Canals			
Transportation			
	Rails		
	Interstate Highways		
	US Routes		
	Major Roads		
	Local Roads		
Background			
	Aerial Photography		
Soil Rating Lines			
	A		
	A/D		
	B		
	B/D		
	C		
	C/D		
	D		
	Not rated or not available		
Soil Rating Points			
	A		
	A/D		
	B		
	B/D		

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Monmouth County, New Jersey
Survey Area Data: Version 13, Sep 16, 2019

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jun 29, 2019—Jul 16, 2019

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher



Natural Resources
Conservation Service

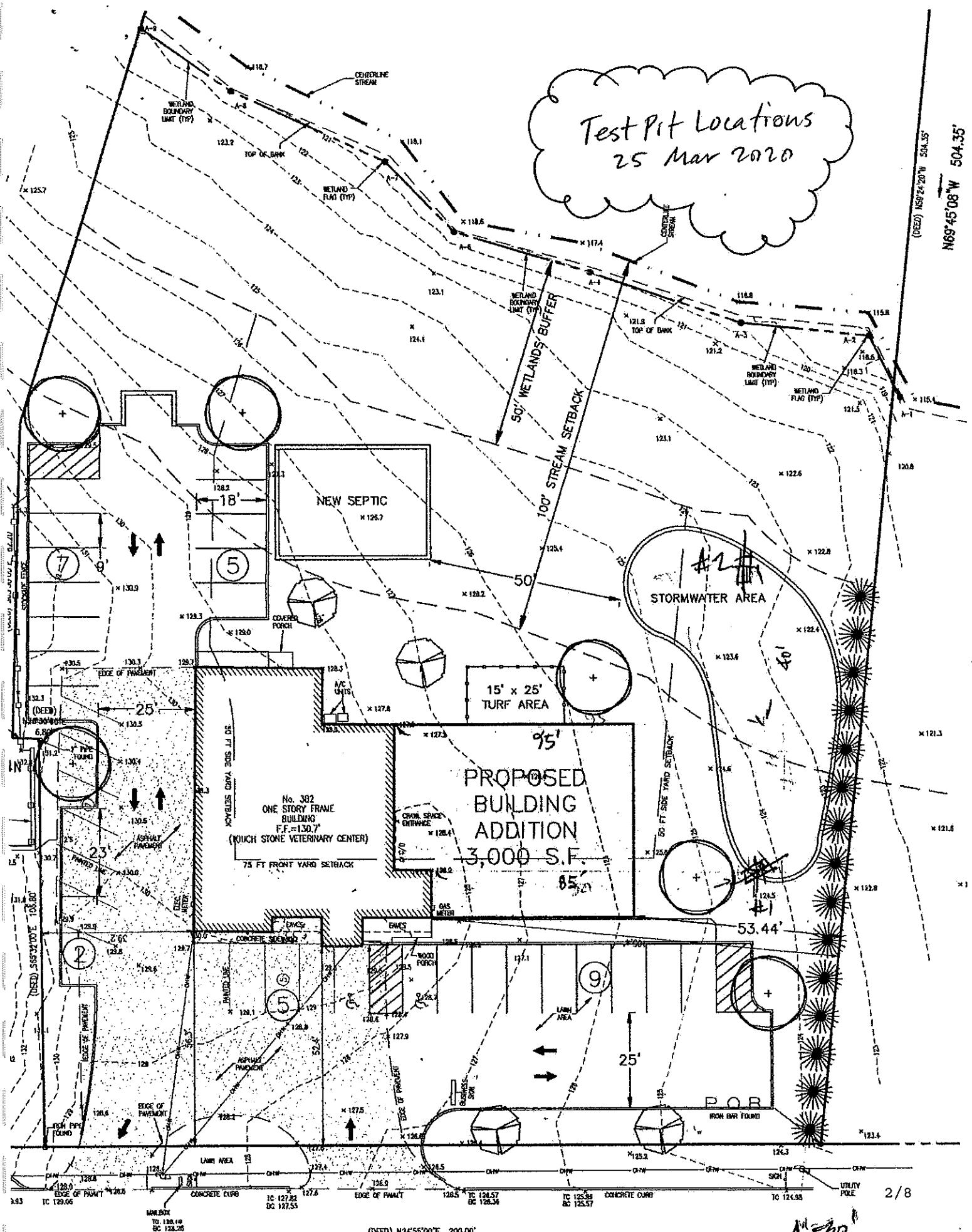
Web Soil Survey
National Cooperative Soil Survey

4/7/2020
Page 4 of 4

N69°45'08"W 504.35'

(DEED) N59°24'20"N 504.35'

Test Pit Locations
25 Mar 2020



MONMOUTH COUNTY / Marlboro Twp.			FORM 3B	7:9A-6.2 TUBE PERMEAMETER TEST	
BLOCK / LOT Block 153 / Lot 12 # 382 rd. 79					
SAMPLE / DEPTH brown SP-SM 2' depth @ test pit #2					
SAMPLE DIMENSIONS			A	B	
RADIUS OF SAMPLE TUBE, CM			3.6 cm	3.6 cm	
LENGTH OF SAMPLE, INCHES A 82/25.4			3.2"	3.0"	
B 76/25.9					
SAMPLE VOLUME, CC			333.9 cc	309.4 cc	
SAMPLE WEIGHT, GRAMS A 523.2 - 7.6			515.6 gr	499.3 gr	
B 456.9 - 7.6					
BULK DENSITY, GRAMS/CC			1.54 gr/cc	1.45 gr/cc	
HEIGHT OF WATER ABOVE RIM, MM					
BEGINNING OF INTERVAL, H1			67	70	
END OF INTERVAL, H2			56	53	
			Ha	Hb	
TIME OF TEST INTERVAL, HH:MM:SS			15:37:00	67	16:07:00
			38	64	12:00
			39	61	12:30
			40	59	17:30
			41	57	H1 18:00
			42	55	H2 23:00
			42:15	67	
			47:15	56	
			H1 48:00	67	
			H2 53:00	56	
INTERVAL, MIN. MIN			5.0	5.0	
CALCULATION OF PERMEABILITY			A: $60 \times 3.2 \times \ln(67/56) / 5.0 = 6.9 \text{ in/hr}$		
			B: $60 \times 3.0 \times \ln(70/53) / 5.0 = 10.0 \text{ in/hr}$		
K, INCHES/HOUR=60 X LENGTH X LN(H1/H2) / TIME					
DEFECTS IN SAMPLE:			OK	OK	
PERMEABILITY RATING			V4 6-20" / hr	K4 6-20" / hr	
I HEREBY CERTIFY THAT THE INFORMATION FURNISHED ON THIS FORM OF THIS APPLICATION IS TRUE AND ACCURATE - I AM AWARE THAT FALSIFICATION OF DATA IS A VIOLATION OF THE WATER POLLUTION CONTROL ACT NJSA 58:10A-1 ET SEQ SUBJECT TO PENALTIES AS PRESCRIBED IN NJAC 7:14-8					
DATE:	26 Mar 2020				6/8
<i>William F. McHeffey</i>					
WILLIAM F. MC HEFFEY, PE, PP			MC ENGINEERING 1041 HWY 36 - STE 202		
NJ 24GE03346600 & 33L100448800			ATLANTIC HIGHLANDS, NJ 07716 (732) 291-4110		

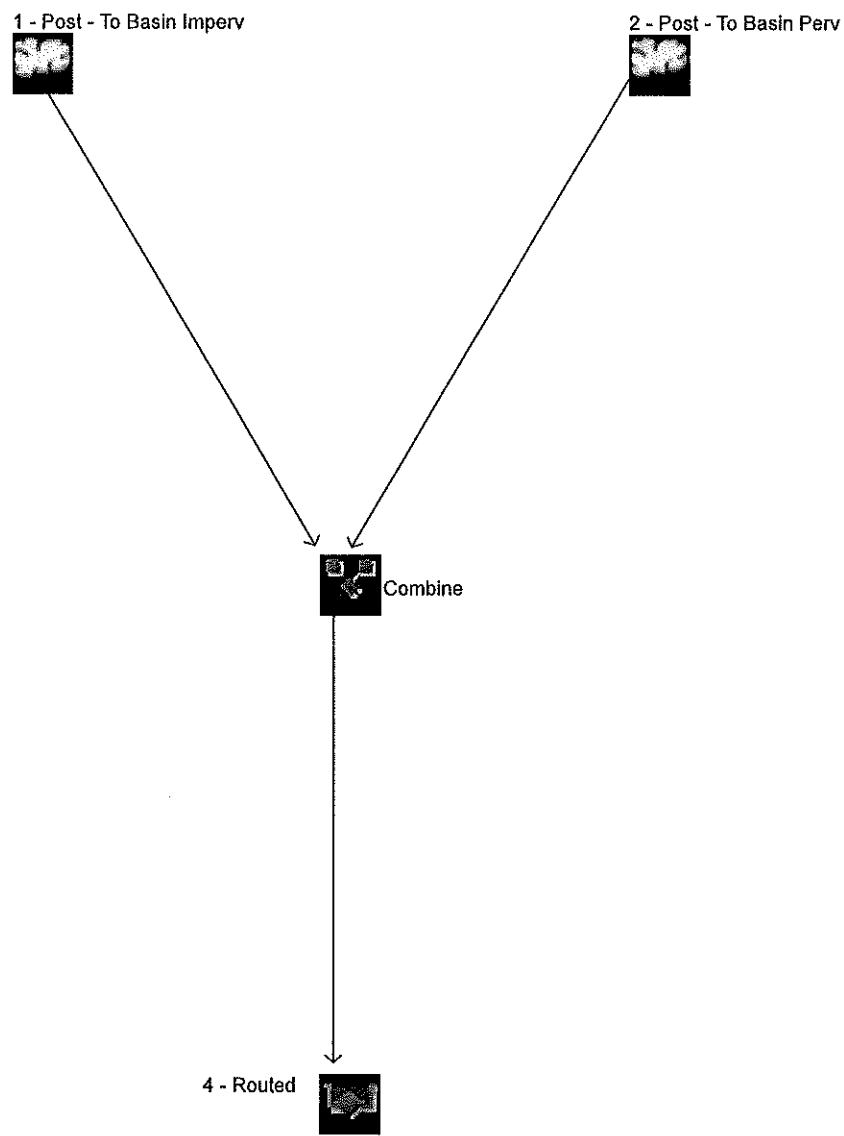


03.25.2020 07:33

TEST PIT #2 EXCAVATION

Watershed Model Schematic

Hydraflow Hydrographs by InteliSolve v9.23



Legend

Hyd. Origin	Description
-------------	-------------

- | | | |
|---|------------|------------------------|
| 1 | SCS Runoff | Post - To Basin Imperv |
| 2 | SCS Runoff | Post - To Basin Perv |
| 3 | Combine | Combine |
| 4 | Reservoir | Routed |

Hydrograph Summary Report

Hydraflow Hydrographs by Infelisolve v9.23

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	0.909	5	70	1,443	---	----	----	Post - To Basin Imperv
2	SCS Runoff	0.020	5	75	41	---	----	----	Post - To Basin Perv
3	Combine	0.924	5	70	1,484	1, 2	----	----	Combine
4	Reservoir	0.062	5	120	1,483	3	122.41	1,172	Routed
proposed 04-07-20 WQ.gpw				Return Period: 1 Year				Thursday, May 14, 2020	

Hydrograph Report

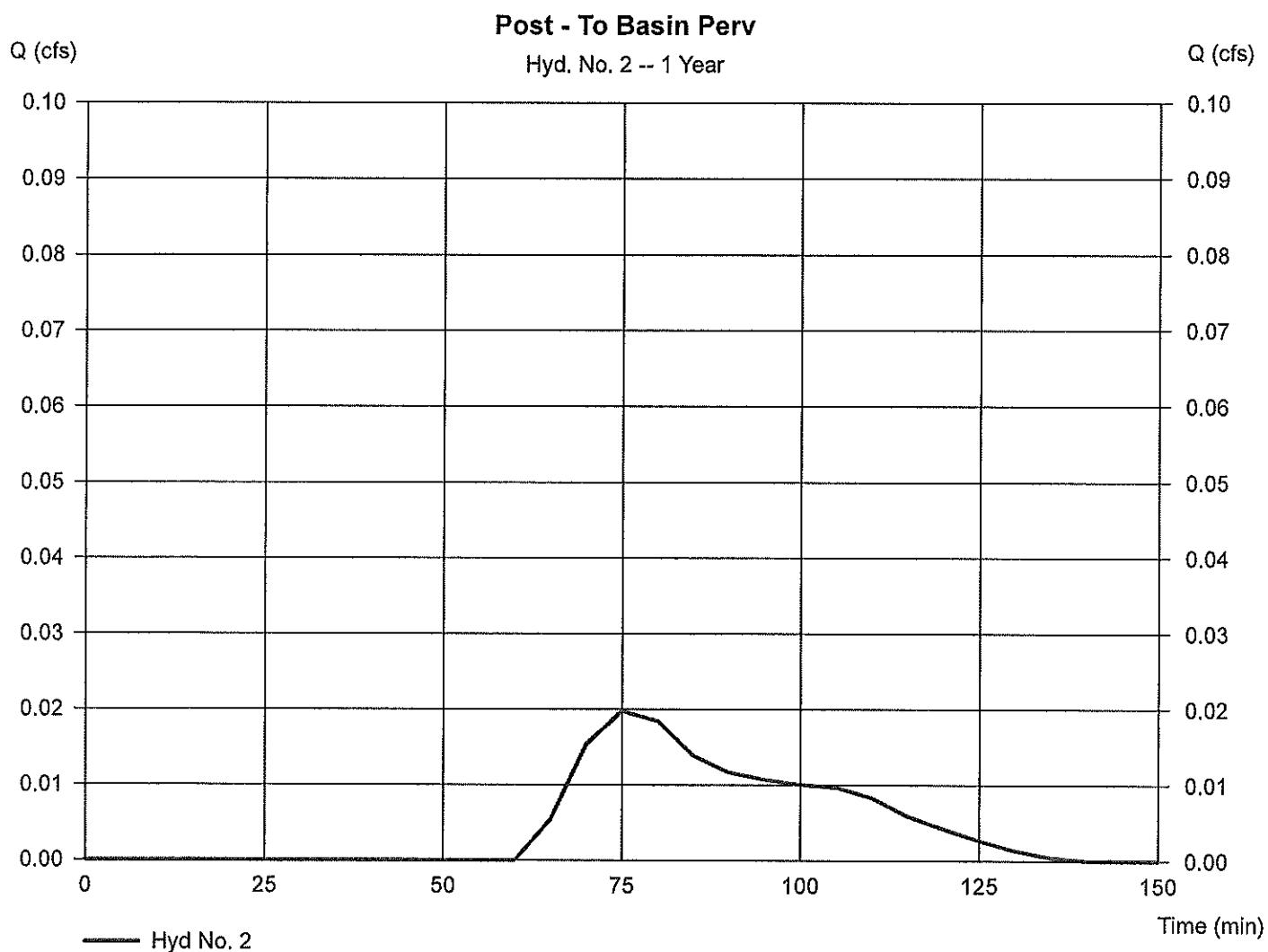
Hydraflow Hydrographs by Intellsolve v9.23

Thursday, May 14, 2020

Hyd. No. 2

Post - To Basin Perv

Hydrograph type	= SCS Runoff	Peak discharge	= 0.020 cfs
Storm frequency	= 1 yrs	Time to peak	= 75 min
Time interval	= 5 min	Hyd. volume	= 41 cuft
Drainage area	= 0.120 ac	Curve number	= 76
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= USER	Time of conc. (Tc)	= 10.00 min
Total precip.	= 1.25 in	Distribution	= Custom
Storm duration	= njdep wq.cds	Shape factor	= 484



Hydrograph Report

Hydraflow Hydrographs by InteliSolve v9.23

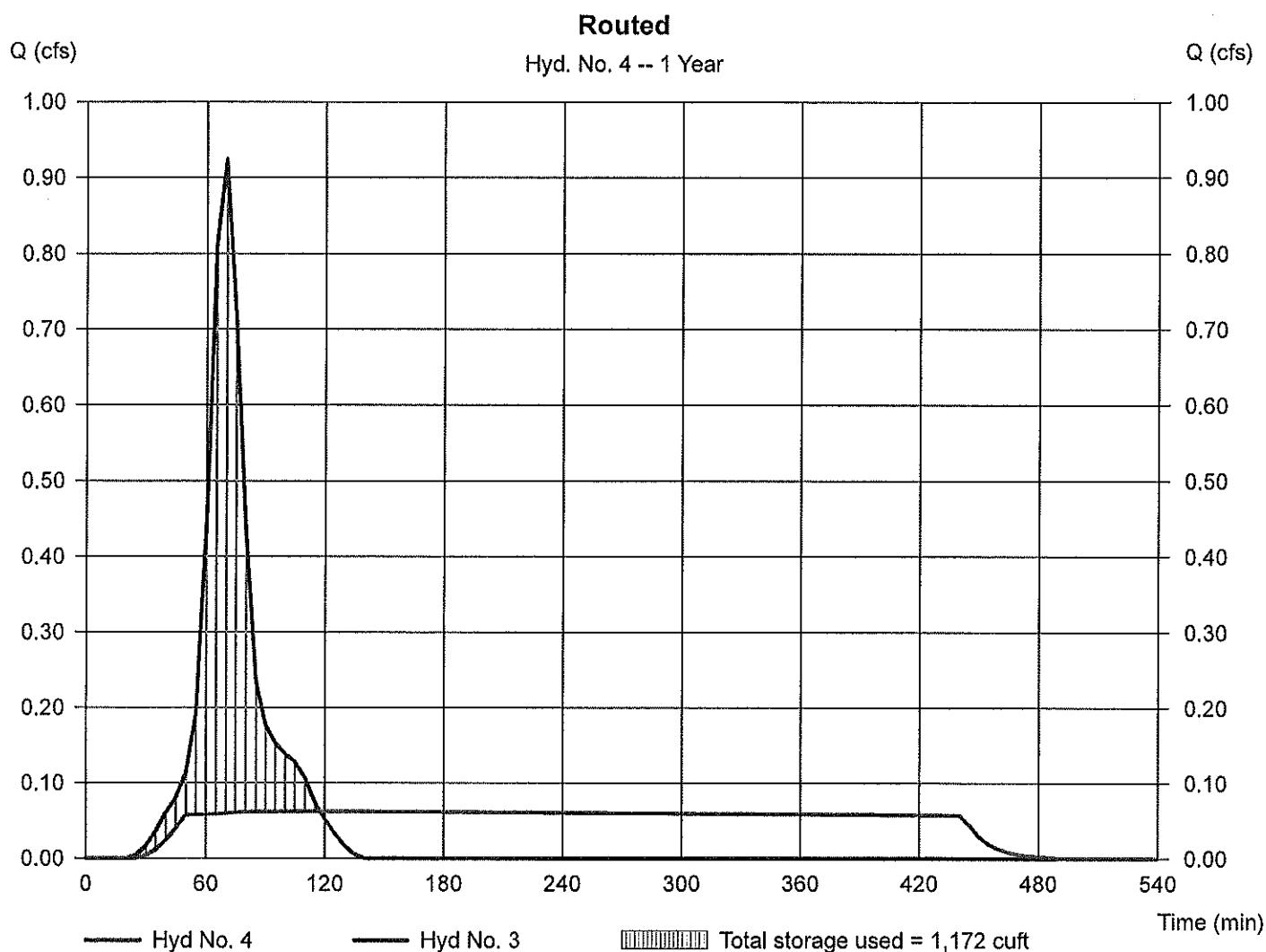
Thursday, May 14, 2020

Hyd. No. 4

Routed

Hydrograph type	= Reservoir	Peak discharge	= 0.062 cfs
Storm frequency	= 1 yrs	Time to peak	= 120 min
Time interval	= 5 min	Hyd. volume	= 1,483 cuft
Inflow hyd. No.	= 3 - Combine	Max. Elevation	= 122.41 ft
Reservoir name	= Basin	Max. Storage	= 1,172 cuft

Storage Indication method used. Outflow includes exfiltration.



Appendix 5

Groundwater Recharge Spreadsheet

Project Name	Description	Analysis Date	BMP or LID Type
Site Plan		04/07/20	Above Ground Detention Basin
Recharge BMP Input Parameters			
Parameter	Symbol	Value	Unit
BMP Area	ABMP	2477.0	sq.ft
BMP Effective Depth, This is the design variable Upper level of the BMP surface (negative if above ground)	dBMP	0.8	in
Depth of lower surface of BMP, must be >=dBMP	dBMPu	-23.4	in
Post-development Land Segment Location of BMP, Input Zero if location is distributed or undetermined	SegBMP	3	unitless

BMP Calculated Size Parameters

ABMP/Aimp	Area	0.154	unlless
BMP Volume	V/BMP	154	c.f.t
Parameters from Annual Recharge Worksheet			
Post-D Deficit Recharge (or desired recharge volume)	Vdef	12,366	c.u.ft
Post-D Impervious Area (or target impervious area)	Aimp	23,087	sq.ft
Root Zone Water Capacity	RWC	0.00	in
RWC Modified to consider dEXC	DRWC	0.00	in
Climatic Factor	C-factor	1.44	no units
Average Annual P	Pavg	44.9	in
Recharge Requirement over Imp. Area	dr	6.4	in

CALCULATION CHECK MESSAGES

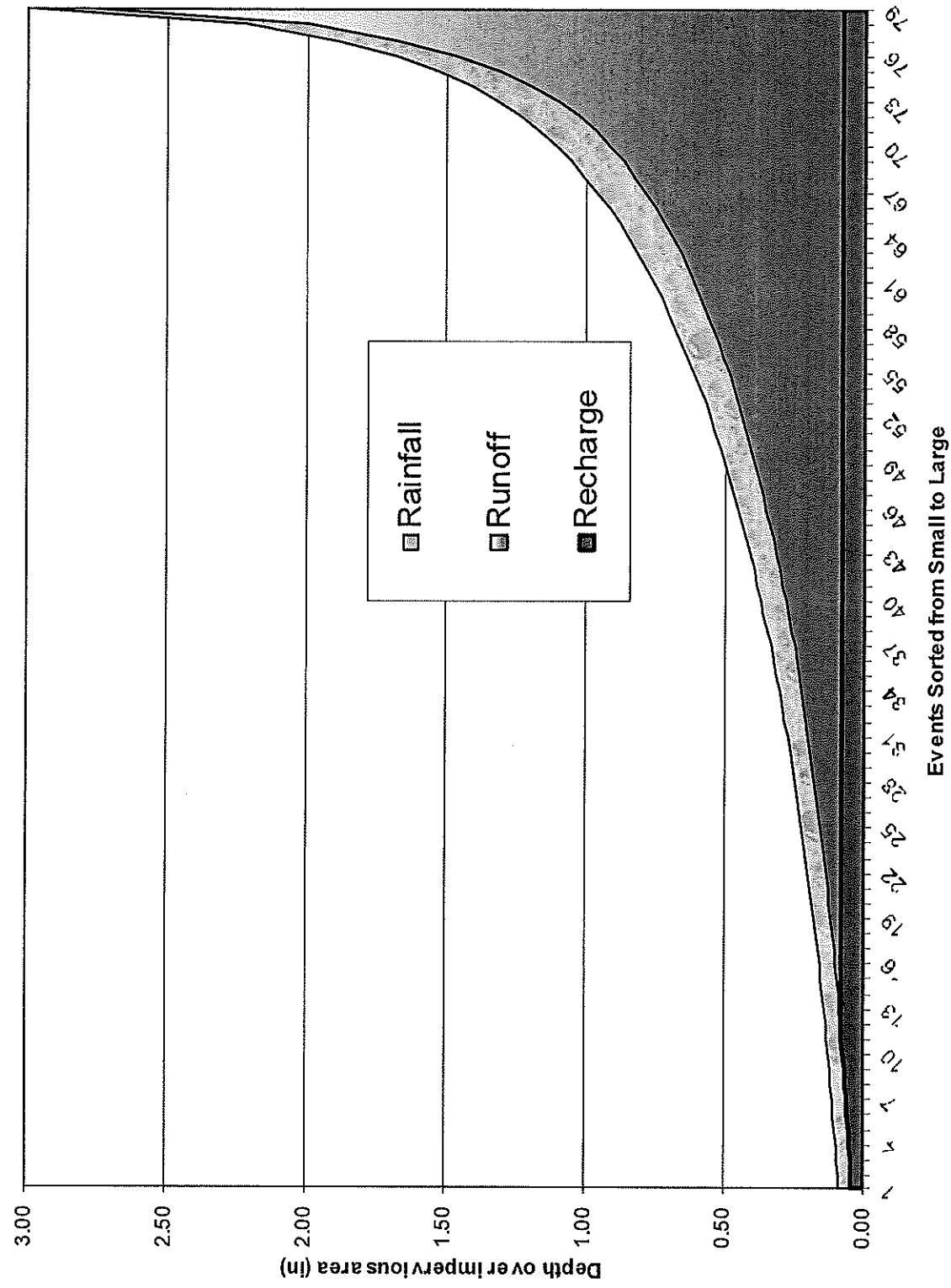
Volume Balance->OK
dBMP Check-> OK
dEXC Check-> OK

BMP Location—> OK

OTHER NOTES

ReDesign is accurate only after BMP dimensions are updated to make tech volume= deficit volume
of BMP Infiltration prior to filling and the area occupied by BMP are ignored in these calculations
sensitive to dBMP, make sure dBMP selected is small enough for BMP to empty in less than 3
Segment Location of BMP if you select "Impervious areas" RWC will be minimal but not zero as

the soil type and a shallow root zone for this Land Cover allowing consideration of lateral flow air
How to solve for different recharge volumes: By default the spreadsheet assigns the values of total deficit recharge volume "Vdef" and total proposed impervious area "Aimp" from the "Annual
Recharge" sheet to "Vdef" and "Aimp" on this page. This allows solution for a single BMP to handle the entire recharge requirement assuming the runoff from entire impervious area is available to the BMP.
To solve for a smaller BMP or a LID-LIMP to recharge only part of the recharge requirement, set Vdef to your target value and Aimp to impervious area directly connected to your infiltration facility and then
solve for ABMP or dBMP. To go back to the default configuration click the "Default Vdef & Aimp" button.



Appendix 6

Storm Sewer Pipe Calculations

Storm Sewer Inventory Report

Page 1

Line No.	Alignment					Flow Data					Physical Data					Line ID	
	Distr line No.	Line length (ft)	Defl angle (deg)	Junc type	Known Q (cfs)	Drg area (ac)	Runoff coeff (C)	Inlet time (min)	Invert El Dn (ft)	Line slope (%)	Invert El Up (ft)	Line size (in)	Line type	N value (n)	J-loss coeff (K)	Inlet/Rim El (ft)	
1	End	92.0	179.9	M/H	0.00	0.13	0.99	10.0	122.00	4.00	125.68	12	Cir	0.013	1.00	128.75	A INLET TO BASIN
2	1	19.4	-89.9	M/H	0.00	0.08	0.99	10.0	125.68	0.98	125.87	6	Cir	0.013	1.00	130.00	ROOF TO A INLET

Project File: stormsewers.pt1.stm

Number of lines: 2

Date: 05-14-2020

Hydraflow Storm Sewers 2005

Storm Sewer Tabulation

Page 1

Station	Len	Drng Area	Rnoff coeff	Area x C			Tc	Rain (I)	Total flow	Cap full	Vel	Pipe	Invert Elev		HGL Elev		Line ID					
				Incr	Total	Inlet							Size	Slope (%)	Up (ft)	Dn (ft)	Up (ft)	Dn (ft)				
1	End	92.0	0.13	0.21	0.99	0.13	0.21	10.0	10.1	6.4	1.33	7.12	3.47	12	4.00	125.68	122.00	126.17	122.49	126.00	A INLET TO BASI	
2	1	19.4	0.08	0.08	0.99	0.08	0.08	10.0	10.0	6.4	0.51	0.55	2.59	6	0.98	125.87	125.68	126.37	126.25	130.00	128.75	ROOF TO A INLE

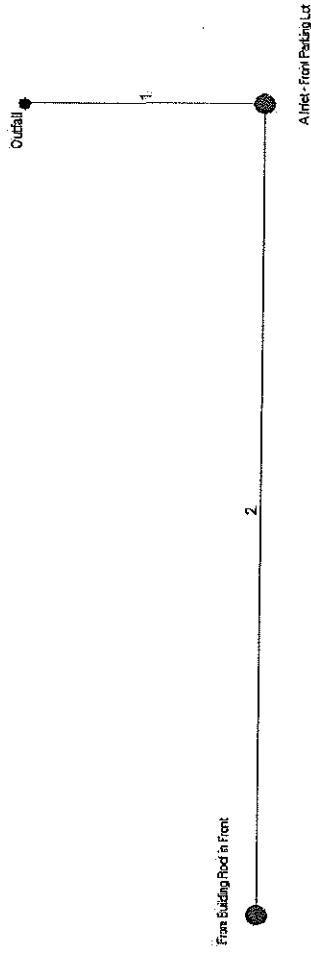
Project File: stormsewers p11.stm

NOTES: Intensity = $125.35 / (\text{Inlet time} + 15.90)^{0.91}$; Return period = 25 Yrs.

Number of lines: 2

Run Date: 05-14-2020

Hydraflow Plan View



382 Route 79

No. Lines: 2

05-14-2020

Storm Sewer Summary Report

Page 1

Line No.	Line ID	Flow rate (cfs)	Line size (in)	Line length (ft)	Invert EL Dn (ft)	Invert EL Up (ft)	Line slope (%)	HGL down (ft)	HGL up (ft)	Minor loss (ft)	HGL Junct (ft)	Dns line No.
1	A INLET TO BASIN	1.10	15 c	44.0	122.00	124.20	5.000	122.42	124.62	n/a	124.62 j	End
2	ROOF TO A INLET	0.44	6 c	164.0	124.20	125.84	1.000	124.68	126.18	n/a	126.18 j	1
382 Route 79					Number of lines: 2				Run Date: 05-14-2020			
NOTES: c = cir; e = ellip; b = box; Return period = 25 Yrs. ;j - Line contains hyd. jump.												

Storm Sewer Profile

Proj. file: stormsewers pt2.stm

Elev. (ft)

